

# PRELIMINARY DRAINAGE REPORT

## The Triangle

7120 E. Indian School Road  
Scottsdale, AZ 85251

Prepared For:

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Project Number: 200504

Revision Date: October 16, 2020 (Rezoning)

Plan #	_____
Case #	10-ZN-2020
Q-S #	_____
<input checked="" type="checkbox"/> Accepted	
<input type="checkbox"/> Corrections	
N. Baronas	11/9/2020
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Case No.: 63-PA-2020  
10-ZN-2020

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## 1. INTRODUCTION

This Preliminary Drainage Report represents the storm water analysis for the HoJo Development (The Triangle) proposed in Scottsdale, Arizona. The purpose of this preliminary report is to provide the hydrologic and hydraulic analysis, required by the City of Scottsdale, to support the proposed rezoning for said development. This report includes discussions and calculations defining the storm water management concepts for the collection and conveyance necessary to comply with the drainage requirements of the City of Scottsdale and Maricopa County. Preparation of this report has been done in accordance with the requirements of the City of Scottsdale Design Standards & Policies Manual (DS&PM) 2018<sup>1</sup>, and the Drainage Design Manuals for Maricopa County, Arizona, Volumes I<sup>2</sup> and Volume II<sup>3</sup>.

## 2. LOCATION AND PROJECT DESCRIPTION

### 2.1 LOCATION:

The subject property consists of land located south of the 3<sup>rd</sup> Avenue and Craftsman Court, the between 3<sup>rd</sup> Avenue and Indian School Road in Scottsdale, AZ:

- A portion of the southeast 1/4 of Section 22, Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian, Maricopa County, Scottsdale, Arizona.
- Parcel ID:      Parcel 173-50-034; The Venue, Zoning C-2 (7117 E. 3<sup>rd</sup> Avenue)  
                      Parcel 173-50-108A; Kimberly at Michael V. Salon, Vape Sky, Teres A Nail Bar, Zoning C-2 (7120 E. Indian School Road, Scottsdale, AZ 85251)  
                      Parcel 173-50-117B; Howard Johnson Inn, Zoning C-2 (7110 E. Indian School Road, Scottsdale, AZ 85251)

Refer to **FIGURE 1 - Vicinity Map** for the project's location with respect to major cross streets

### 2.2 EXISTING AND PROPOSED DEVELOPMENTS SURROUNDING THE SITE:

- West: The site is bound by an alley with the following across as follows:  
                      Parcel 173-50-129; Marshall Way Plaza; Zoning is C-2  
                      Parcel 173-50-114; Pink Plaza; Zoning is C-2
- East: Parcel 173-50-119E, 173-50-094, -100A; commercial shops, Zoning D-/OR-2
- North: Across 3<sup>rd</sup> Avenue: Parcel 173-50-019; Foxy Spray Tans; Zoning is C-2  
                      Across 3<sup>rd</sup> Avenue: Parcel 173-50-146; Cadre Condominiums; Zoning is C-2
- South: Across Indian School Road are parcels:  
                      Parcel 130-12-013, -012, -011; Commercial offices; Zoning is C-2.  
                      Parcel 130-12-007A

### 2.3 EXISTING SITE DESCRIPTION:

The project area includes approximately 144,173 sf. ft. (3.310 acres) of land designated as C-2 per C.O.S. zoning map 5. The site is currently developed and includes three commercial developments with parking lots: Howard Johnson Inn, The Venue and a commercial building comprised of several retail stores. The developments are separated by parking areas.

Per Topographic Survey prepared by AWL Land Surveying, the site slopes from northwest to southeast at approximately 1.00%. Elevation varies from approximately 1266.24 at the northwest corner to approximately 1262.21 at the southeast corner. The site drains to the perimeter streets and alley.

Refer to **FIGURE 2** attached for an aerial of the site.

#### **2.4 PROPOSED SITE DEVELOPMENT:**

Site development includes the demolition of the Howard Johnson Inn, The Venue structures and their designated parking lots as well as the construction of a new hotel, residential building and townhome complex. The development will include one proposed access on the north side to 3<sup>rd</sup> Avenue, two access entrances to the alley on the west, and will maintain the two existing driveway entrances to Indian School Road. An underground parking structure is proposed for the development. Refer to **Appendix III - Preliminary Grading Plan** for site layout.

#### **2.5 FLOOD HAZARD ZONE:**

FIRM Map Number 04013C2235L dated October 16, 2013 indicates the site is designated as Zone "X". As such, it is defined as areas determined to be outside the 0.2% annual chance floodplain and therefore is not in a special flood hazard area.

Refer to **FIGURE 3** for the FIRM.

### **3. EXISTING DRAINAGE CONDITIONS**

#### **3.1 OFF-SITE DRAINAGE PATTERNS**

The topographic survey provides the following information for offsite drainage:

- There is an existing alley to the west approximately 16' wide that slopes from north to south. The alley conveys drainage from the site onto Indian School Road.
- The existing sidewalks to the north and south of the site drain into their adjacent streets, 3<sup>rd</sup> Avenue and Indian School Road, respectively.
- Adjacent roads have curb and gutters conveying flow within the rights-of-way. Flows from Indian School Road are collected in EX. CB-1 and EX. CB-2.
- An existing inlet, EX. CB-3, located east of the EX-3 drainage area concentration point, collects runoff from EX-3 and adjacent parking area. Refer to **Appendix IV** for site photos.
- Based on existing conditions obtained by the topo and site photos, the site sits 1-2' above the pavement grade along the east parcels. Therefore, it was concluded that the existing site is not affected by any offsite flows.
- Refer to Section 5.1 for additional discussion of safety of finish floor elevations.

#### **3.2 ONSITE DRAINAGE**

Based on the topographic information, only drainage areas EX-1 and EX-2 located at the north end of the property drain to 3<sup>rd</sup> Avenue. The runoff along 3<sup>rd</sup> avenue flows east where it is ultimately conveyed onto N. Scottsdale Road. Drainage area EX-3 and EX-4 drain to the neighboring parcel to the east, but ultimately makes their way to Indian School Road. Similarly, drainage area EX-7 drains to the alley adjacent to the west but ultimately discharges to Indian School Road. Drainage areas EX-5 and EX-6 drain to Indian School Road and flows are captured by catch basins along Indian School Road.

Refer to Appendix II for **Existing Conditions Drainage Area Map**.

The Rational Method was utilized to compute the on-site peak discharges. The Rational Method equation is calculated as shown below:

$$Q=C_{wt}IA$$

Where:  $C_{wt}$  = The runoff coefficient relating runoff to rainfall

$I$  = Average rainfall intensity in inches/hour, lasting for  $T_c$

$T_c$  = The time of concentration (using five minutes for the developed areas)

$A$  = The contributing drainage area in acres

Refer to section 4.3 for land characteristics.

Table 1 below is a summary of existing  $Q_{100}$  runoff and required storage volume:

**TABLE 1:**

<b>Existing Runoff Calculations</b>				
Drainage	Area	$C_w$	intensity	Q
Area ID	(acres)	(-)	(in/hr)	(cfs)
<b>Contributing Areas to 3rd Ave</b>				
EX-1	0.20	0.95	7.44	1.41
EX-2	0.67	0.95	7.44	4.74
<b>Totals</b>	<b>0.87</b>	<b>0.95</b>		<b>6.15</b>
<b>Contributing Areas to Indian School Road</b>				
EX-3	0.24	0.95	7.44	1.70
EX-4	0.36	0.95	7.44	2.54
EX-5	0.48	0.94	7.44	3.36
EX-6	1.04	0.87	7.44	6.73
EX-7	0.19	0.95	7.44	1.34
<b>Totals</b>	<b>2.31</b>	<b>0.91</b>		<b>15.67</b>

Overall project area includes **3.18 Acres at  $C_{wt} = 0.92$**  (Existing conditions, to back of sidewalk)

Refer to the **Existing Cwt Exhibit (Exhibit A)** and **Existing Conditions Drainage Area Map (Exhibit C)** in **Appendix II**.

## 4. PROPOSED STORM WATER MANAGEMENT

### 4.1 DESIGN INTENT:

On-site drainage will be directed off-site via overland flow to the historical outlets. This is a re-development of existing commercial land; therefore, the City of Scottsdale specifies that on-site retention shall be provided as described in Section 4.2 below.

The majority of the entire site is proposed impervious with minor increases in runoff compared to existing conditions.

Refer to **Appendix II for Proposed Conditions Drainage Area Map**.

### 4.2 DESIGN STORM REQUIREMENTS:

In accordance with City of Scottsdale requirements, stormwater storage for the 100-year 2-hour storm event is required based on maintaining existing retention volume plus the difference between the pre

vs. post development runoff from the 100-year 2-hour storm event if increased or first flush, whichever is greater.

#### **4.3 LAND CHARACTERISTICS:**

The proposed project site consists mainly of roofs and covered gathering areas, sidewalks and minor landscape areas along the south and north boundaries. Based on the DS&PM, runoff coefficients for the 100-year storm event used are as follows:

- C=0.95 for building or concrete
- C=0.95 for paved surface
- C=0.45 for undisturbed natural desert or desert landscape

**HYDROLOGIC ANALYSIS:** The hydrologic analysis is determined using the procedures in the City of Scottsdale Design Standards & Policies Manual and the Drainage Design Manual for Maricopa County, Arizona, Volume I. The Rational Method was utilized to compute the on-site peak discharges. The Rational Method equation is displayed as shown below:

$$Q=C_{wt}IA$$

Where:  $C_{wt}$  = The runoff coefficient relating runoff to rainfall

I = Average rainfall intensity in inches/hour, lasting for  $T_c$

$T_c$  = The time of concentration (Using Five minutes for the developed areas)

A = The contributing drainage area in acres

Table 2 below is a summary of Proposed  $Q_{100}$  runoff.

**TABLE 2:**

<b>Proposed Runoff Calculations</b>				
Drainage	Area	$C_w$	intensity	Q
<u>Area ID</u>	(acres)	(-)	(in/hr)	(cfs)
<b>Contributing Areas to 3rd Ave</b>				
DA-1	0.37	0.95	7.44	2.62
DA-2	0.47	0.93	7.44	3.25
<b>Totals</b>	<b>0.84</b>	<b>0.94</b>		<b>5.87</b>
<b>Contributing Areas to Indian School Road</b>				
DA-3	1.13	0.95	7.44	7.99
DA-4	0.48	0.95	7.44	3.39
DA-5	0.46	0.91	7.44	3.11
DA-6	0.27	0.95	7.44	1.91
<b>Totals</b>	<b>2.34</b>	<b>0.94</b>		<b>16.40</b>

Overall project area includes **3.18 Acres at  $C_{wt} = 0.94$**  (Proposed conditions, to back of curb)

Refer to the **Proposed Cwt Exhibit (Exhibit B)**, **Proposed Conditions Drainage Area Map (Exhibit D)** and Calculations in **Appendix II**.

Table 5 summarizes the calculated onsite peak flows for the 100-yr storm event under proposed and existing conditions.

**TABLE 3:**

Runoff Calculations Summary			
Outfall	Proposed	Existing	Difference
3rd Avenue	5.87	6.15	-0.28
Indian School Road	16.40	15.67	0.73

The increase in flow to Indian School Road is less than 1 cfs and the storm drains have the capacity to accommodate the project flow based on calculations in Appendix II and Section 4.6.

#### 4.4 STORMWATER RETENTION:

**PRE VS POST:** Based on topographic survey there is no retention provided on the existing development. Based on the performed calculations above, existing condition and proposed development storage requirements for the 100-yr, 2-hr storm event are calculated as follows:

**TABLE 4:**

Pre vs. Post Required Storage Volume Calculation Summary					
$V = A * (C_{wpost} - C_{wpre}) * D / 12$					
Area	$C_{wpost}$	$C_{wpre}$	Depth	Volume Req.	
(acres)	(-)	(-)	(in)	(acre-ft)	(CF)
3.18	0.94	0.92	2.16	0.011	498.67

**FIRST FLUSH:** First Flush storage required is calculated in accordance with COS– DS&PM. According to the DS&PM, sites less than one (1) acre in size may be waived from the First Flush requirement with approval from staff. The area considered in the first flush calculation is the disturbed area minus any true roof top area. As shown in the Proposed Conditions Roof Area Exhibit (Exhibit E) in Appendix II, the areas considered in the first flush calculation (**0.92 ac**) quantified to be less than 1 acre. As such, the site could be considered exempt from the first flush requirement.

Refer to **Proposed Conditions Roof Area Exhibit (Exhibit E)** in Appendix II for areas considered in the first flush calculation.

#### 4.5 STORMWATER RETENTION WAIVER:

The proposed development includes an underground parking structure to the limits of the property thereby eliminating potential open or underground retention areas. Runoff to the north (3<sup>RD</sup> Avenue) is reduced by 0.28 cfs. The total increase to the south (Indian School Road) is 0.73 cfs and the street and storm drains have capacity to accommodate the project flows based on projected peak flows in Table 3 and offsite flows presented in section 4.6. First flush treatment is not required. Therefore, a Request for Stormwater Storage Waiver for 499 cf will be applied for based on section 4-1.203 DS&PM. Refer to **Appendix IV** for Stormwater Retention Waiver.

#### 4.6 OFFSITE STORM SYSTEM ANALYSIS:

For the purpose of this report, the calculated runoff was used to analyze the effects of the increase in runoff to the existing system based on the existing peak flows presented in the Lower Indian Bend Wash Area Drainage Master Study Hydrology and Hydraulics Report, Contract No.: FCD 2011C019, dated December 2017.

The hydraulic grade line and capacity was analyzed for the existing 48" RGRCP reach along E. Indian School Road. The reach begins at the upstream manhole, MJ8W2STEISRL, located at the Alley and E. Indian School Road intersection and continues east to N Scottsdale Road at manhole MJ23W2STSRL, refer to Appendix V for an excerpt of the Lower Indian Bend Wash ADMP corresponding to the analyzed reach along Indian School Road.

The onsite peak flows from Table 6 were calculated through the use of the Rational Method and indicate that there is a 0.73 cfs increase to Indian School Road. The hydraulic analysis was performed for the existing 36" storm drain (upstream) and the 48" (downstream) to verify the capacity of the existing system in respect to the additional flow. The analysis was performed using Flowmaster to analyze the existing 36" and 48" RGRCP reach based on the existing peak flow of 32.4 cfs and 71.5 cfs at pipes **C6W2STEISRL** and **C1W2STEISRL**, respectively, obtained from the Lower Indian Bend Wash ADMP, and the additional 0.73 cfs obtained from the calculated on-site peak flow. Refer to **Appendix V** for Inlet Summary Table and Pipe Discharge Tables in the Lower Indian Bend Wash ADMP.

$$36" \text{ Pipe C6W2STEISRL: } 32.4 \text{ cfs (Existing)} + 0.73 \text{ cfs (Post)} = \mathbf{33.13 \text{ cfs}}$$
$$48" \text{ Pipe C1W2STEISRL: } 71.5 \text{ cfs (Existing)} + 0.73 \text{ cfs (Post)} = \mathbf{72.23 \text{ cfs}}$$

Hydraulic calculations indicate that 52.94 cfs is available for the existing 36" RGRCP ( $S=0.63\%$ ) at full capacity and 114.01 cfs available for the existing 48" RGRCP ( $S=0.63\%$ ) at full capacity. The existing 36" and 48" RGRCP storm drains are capable of conveying the total post conditions flow increase of 0.73 cfs. Refer to **Appendix II** for pipe capacity calculations.

#### **4.7 ADEQ WATER QUALITY REQUIREMENTS:**

The total disturbed area of this site is approximately 3.18 acres. The Arizona Department of Environmental Quality requires that any site disturbance over an acre is required to submit an NOI. An NOI will be submitted to ADEQ for this site after the first submittal of the construction documents as this site disturbance is over 1 acre.

## **5. FLOOD SAFETY FOR DWELLINGS**

### **5.1 FINISHED FLOOR ELEVATIONS**

This project lies in an "X" Flood Zone. Therefore, the proposed building finished floor elevations will be set a minimum of 12 inches above the 100-year high-water elevation of any adjacent streets and drainage paths and a minimum of 14 inches above the lowest top of curb of the lot. This will ensure that each building will be well above the 100-year water level. All buildings with the exception of Buildings 4 and 5 are set 14 inches above the lowest top of curb but are set more than 12 inches above the 100-year water surface elevation at the ultimate outfall. The site ultimate outfall is located at the southeast corner at an elevation of 1261.15. The ultimate outfall elevation is greater than 14" below the minimum finish floor elevation.

**TABLE 5:**

FFE Summary			
BLDG	Finish Floor Elevation	Lowest Top of Curb	Difference
(ID)	(ft)	(ft)	(in)
1	66.00	64.62	16.56
2	66.00	64.42	18.96
3	66.00	62.81	38.28
4	65.00	64.20	9.60
5	65.00	63.98	12.24
6	64.50	62.40	25.20

## 6. CONCLUSIONS

### 6.1 OVERALL PROJECT:

1. The finish floor elevations will be designed a minimum of 12 inches above the 100-year water surface in adjacent streets and drainage paths and a minimum of 14 inches above the lowest top of curb of the lot.
2. A stormwater storage waiver will be requested for the redevelopment of the site.

### 6.2 PROJECT PHASING:

This project will be constructed in a single phase.

## 7. WARNING AND DISCLAIMER OF LIABILITY

RE: following page.

## 8. REFERENCES

1. *Design Standards & Policies Manual, City of Scottsdale – January 2018*
2. *Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology, Flood Control District of Maricopa County, Fourth Edition, December 14, 2018*
3. *Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics, Flood Control District of Maricopa County, December 14, 2018*

# GRADING & DRAINAGE LANGUAGE

## WARNING AND DISCLAIMER OF LIABILITY

The City's Stormwater and Floodplain Management Ordinance is intended to minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding.

The Stormwater and Floodplain Management Ordinance identifies floodplains, floodways, flood fringes and special flood hazard areas. However, a property outside these areas could be inundated by floods. Also, much of the city is a dynamic flood area; floodways, floodplains, flood fringes and special flood hazard areas may shift from one location to another, over time, due to natural processes.

### WARNING AND DISCLAIMER OF LIABILITY

The flood protection provided by the Stormwater and Floodplain Management Ordinance is considered reasonable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by constructed or natural causes. The Stormwater and Floodplain Management Ordinance does not create liability on the part of the city, any officer or employee thereof, or the federal, state or county government for any flood damages that result from reliance on the Ordinance or any administrative decision lawfully made thereunder.

Compliance with the Stormwater and Floodplain Management Ordinance does not ensure complete protection from flooding. Flood-related problems such as natural erosion, streambed meander, or constructed obstructions and diversions may occur and have an adverse effect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations.

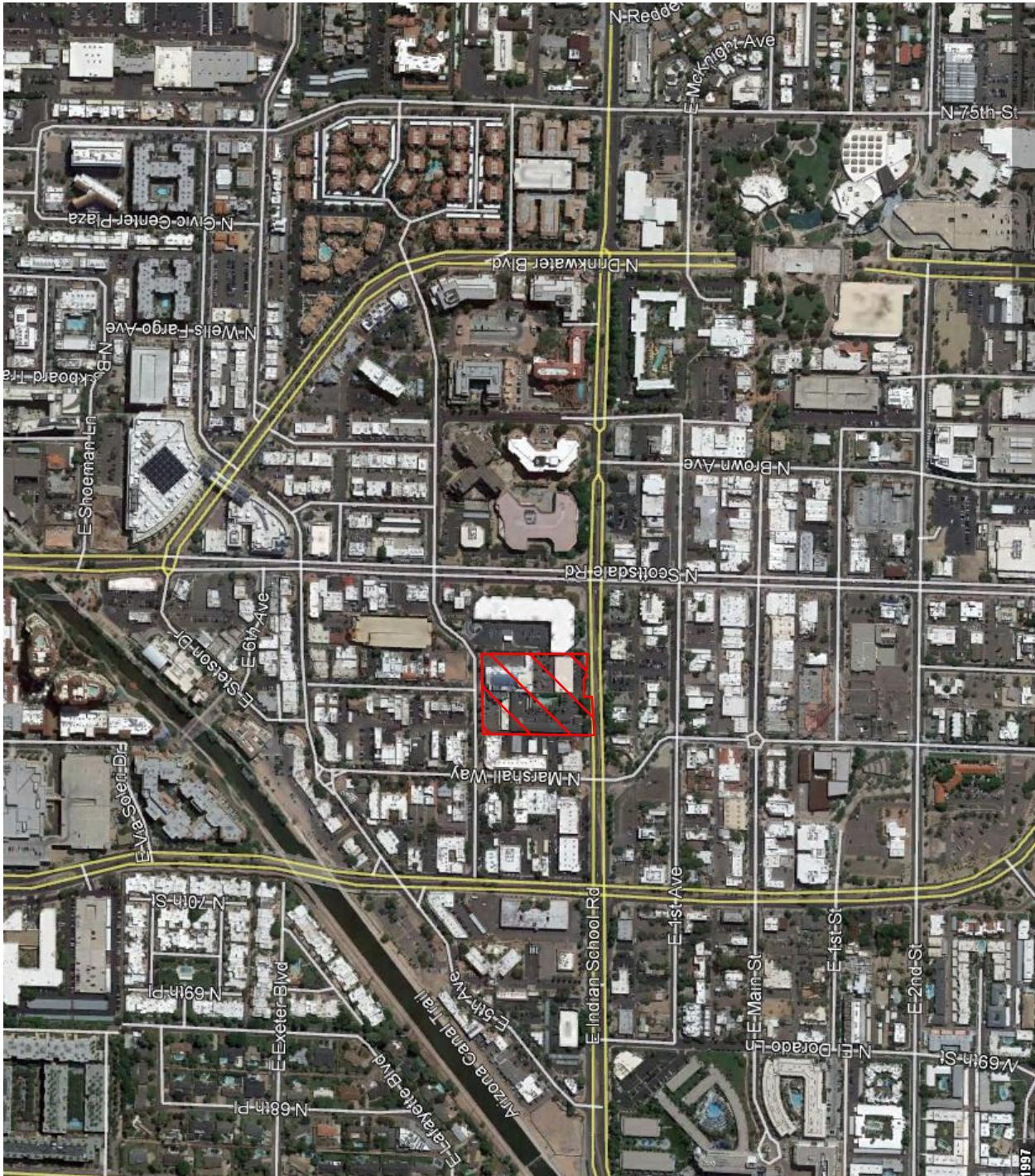
I have read and understand the above.

Plan Check #

Owner

Date

**FIGURE 1**  
VICINITY MAP





**FIGURE 2**  
AERIAL MAP

8280 E. Gelding Dr., Suite 101  
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Sustainability Engineering Group  
10/22/20

PROJECT  
SITE

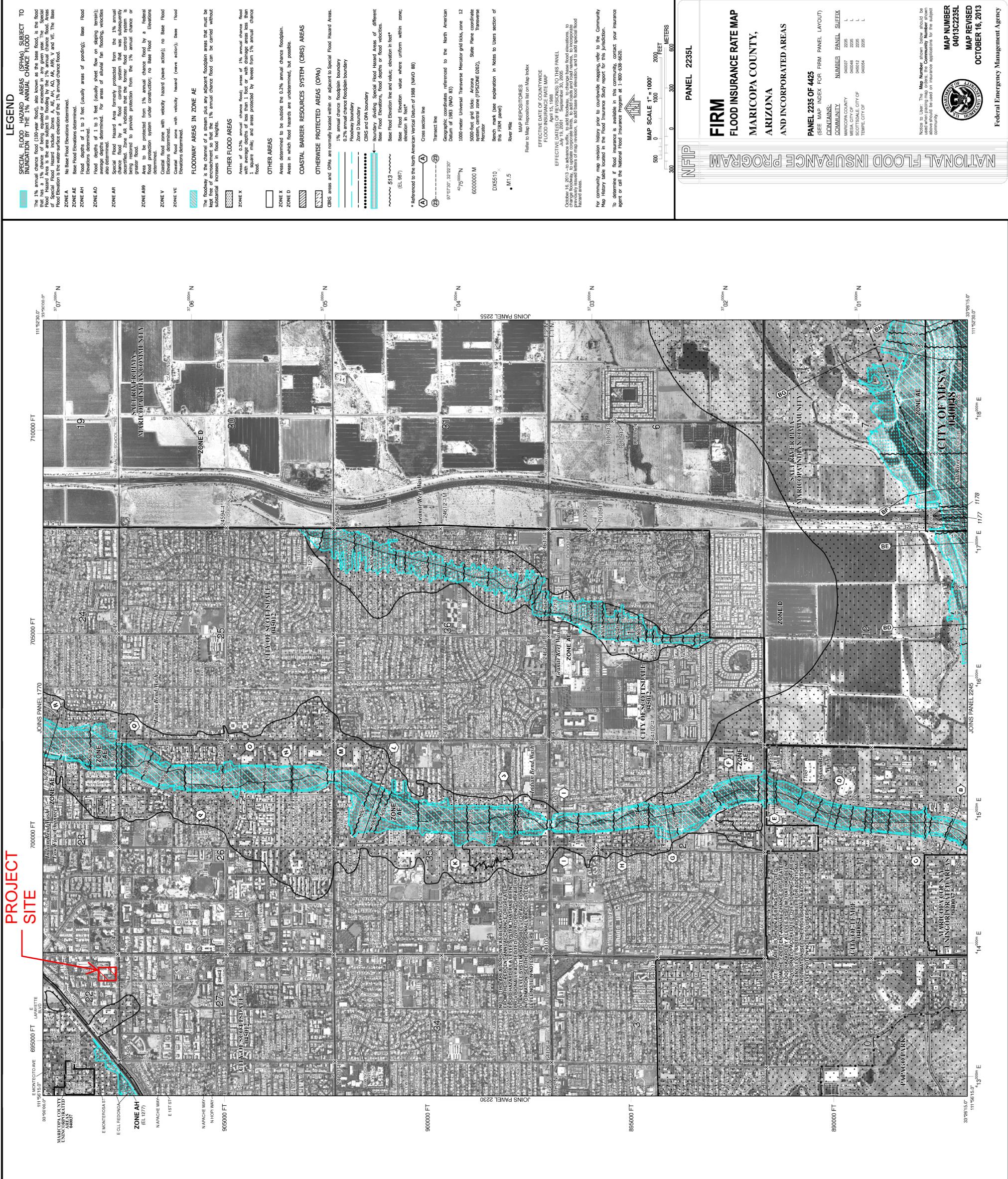
This map is for use in an insurance program. It does not necessarily show areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible up-to-date flood hazard information.

The Department (AHTS) and is dated 2007. The duration of the digital FIRM is State Plane NAD 1983. The map represents the hydraulic modelling results from the FIS report. As a result of improved modelling methods, in some cases, may deviate significantly from the SFWHA.

The base map is based on the best data available at the time of compilation. It is the user's responsibility to determine if the data is suitable for use in annexations or de-annexations. If you have any questions regarding the data, please contact appropriate state or local officials.

**Map Index** for an overview map of the community map repository addresses; containing National Flood Insurance Program a listing of the panels on which each

**Provisionally Accredited Levee Notes to Users:** Check with your local community to obtain more information, such as the estimated level at protection provided (which may exceed the 1-percent-annual-chance level) and Emergency Action Plan on the levee system it is shown as providing protection for areas on this panel, to maintain accreditation. The levee owner or community is required to submit this data and documentation necessary to comply with Section 65.0 of the NFIP regulations by June 25, 2011. If the community or owner does not provide the necessary data and documentation or if the data and documentation provided indicate the levee system does not comply with Section 65.0 requirements, FEMA will revise the flood hazard and risk information for this area to reflect changes in the levee system to mitigate flood risk residual risk areas, property owners and residents are encouraged to consider flood insurance and floodproofing and other protective measures. For more information on flood



**FIGURE 3**  
**FEMA FIRMS**

## *APPENDIX I*

### *Rainfall Data*

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APPENDIX 10-ZN-2020  
10/22/20

**NOAA Atlas 14, Volume 1, Version 5****Location name: Scottsdale, Arizona, USA\*****Latitude: 33.4955°, Longitude: -111.9279°****Elevation: 1262.91 ft\*\***

\* source: ESRI Maps

\*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)
**PF tabular**

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.183</b> (0.154-0.223)	<b>0.240</b> (0.202-0.292)	<b>0.326</b> (0.273-0.395)	<b>0.392</b> (0.326-0.473)	<b>0.481</b> (0.393-0.578)	<b>0.550</b> (0.444-0.658)	<b>0.620</b> (0.492-0.740)	<b>0.693</b> (0.539-0.825)	<b>0.789</b> (0.598-0.941)	<b>0.862</b> (0.641-1.03)
10-min	<b>0.279</b> (0.234-0.340)	<b>0.365</b> (0.307-0.444)	<b>0.496</b> (0.415-0.602)	<b>0.596</b> (0.496-0.720)	<b>0.733</b> (0.599-0.880)	<b>0.838</b> (0.676-1.00)	<b>0.944</b> (0.748-1.13)	<b>1.05</b> (0.821-1.26)	<b>1.20</b> (0.910-1.43)	<b>1.31</b> (0.976-1.57)
15-min	<b>0.345</b> (0.290-0.421)	<b>0.452</b> (0.381-0.550)	<b>0.614</b> (0.514-0.746)	<b>0.739</b> (0.614-0.893)	<b>0.908</b> (0.742-1.09)	<b>1.04</b> (0.838-1.24)	<b>1.17</b> (0.927-1.40)	<b>1.31</b> (1.02-1.56)	<b>1.49</b> (1.13-1.78)	<b>1.63</b> (1.21-1.95)
30-min	<b>0.465</b> (0.390-0.567)	<b>0.609</b> (0.513-0.741)	<b>0.827</b> (0.692-1.00)	<b>0.995</b> (0.827-1.20)	<b>1.22</b> (0.999-1.47)	<b>1.40</b> (1.13-1.67)	<b>1.58</b> (1.25-1.88)	<b>1.76</b> (1.37-2.10)	<b>2.00</b> (1.52-2.39)	<b>2.19</b> (1.63-2.62)
60-min	<b>0.576</b> (0.483-0.702)	<b>0.754</b> (0.635-0.917)	<b>1.02</b> (0.857-1.24)	<b>1.23</b> (1.02-1.49)	<b>1.51</b> (1.24-1.82)	<b>1.73</b> (1.40-2.07)	<b>1.95</b> (1.55-2.33)	<b>2.18</b> (1.70-2.60)	<b>2.48</b> (1.88-2.96)	<b>2.71</b> (2.02-3.24)
2-hr	<b>0.667</b> (0.569-0.796)	<b>0.864</b> (0.736-1.03)	<b>1.16</b> (0.983-1.38)	<b>1.38</b> (1.16-1.64)	<b>1.69</b> (1.40-1.99)	<b>1.92</b> (1.57-2.26)	<b>2.16</b> (1.74-2.54)	<b>2.41</b> (1.91-2.83)	<b>2.74</b> (2.12-3.22)	<b>2.99</b> (2.26-3.54)
3-hr	<b>0.726</b> (0.615-0.873)	<b>0.931</b> (0.793-1.13)	<b>1.22</b> (1.04-1.47)	<b>1.46</b> (1.22-1.74)	<b>1.78</b> (1.47-2.12)	<b>2.04</b> (1.66-2.42)	<b>2.31</b> (1.85-2.74)	<b>2.59</b> (2.04-3.07)	<b>2.98</b> (2.28-3.53)	<b>3.30</b> (2.46-3.91)
6-hr	<b>0.874</b> (0.757-1.03)	<b>1.11</b> (0.963-1.30)	<b>1.42</b> (1.23-1.67)	<b>1.67</b> (1.43-1.95)	<b>2.01</b> (1.70-2.33)	<b>2.28</b> (1.90-2.63)	<b>2.56</b> (2.10-2.95)	<b>2.84</b> (2.28-3.29)	<b>3.23</b> (2.53-3.75)	<b>3.54</b> (2.71-4.11)
12-hr	<b>0.977</b> (0.855-1.14)	<b>1.24</b> (1.08-1.44)	<b>1.57</b> (1.36-1.81)	<b>1.83</b> (1.58-2.11)	<b>2.17</b> (1.86-2.50)	<b>2.44</b> (2.07-2.81)	<b>2.72</b> (2.27-3.13)	<b>3.00</b> (2.47-3.45)	<b>3.38</b> (2.71-3.91)	<b>3.67</b> (2.89-4.27)
24-hr	<b>1.17</b> (1.04-1.32)	<b>1.48</b> (1.32-1.67)	<b>1.92</b> (1.71-2.17)	<b>2.27</b> (2.02-2.55)	<b>2.75</b> (2.42-3.09)	<b>3.13</b> (2.74-3.51)	<b>3.53</b> (3.07-3.96)	<b>3.94</b> (3.40-4.42)	<b>4.51</b> (3.85-5.06)	<b>4.96</b> (4.19-5.58)
2-day	<b>1.26</b> (1.13-1.42)	<b>1.61</b> (1.44-1.82)	<b>2.12</b> (1.89-2.38)	<b>2.52</b> (2.24-2.83)	<b>3.08</b> (2.72-3.46)	<b>3.53</b> (3.10-3.96)	<b>4.00</b> (3.49-4.50)	<b>4.50</b> (3.89-5.06)	<b>5.19</b> (4.44-5.85)	<b>5.74</b> (4.86-6.49)
3-day	<b>1.33</b> (1.19-1.50)	<b>1.71</b> (1.52-1.92)	<b>2.25</b> (2.00-2.53)	<b>2.68</b> (2.37-3.01)	<b>3.29</b> (2.90-3.69)	<b>3.78</b> (3.31-4.24)	<b>4.30</b> (3.74-4.83)	<b>4.85</b> (4.18-5.45)	<b>5.62</b> (4.79-6.32)	<b>6.24</b> (5.26-7.04)
4-day	<b>1.41</b> (1.25-1.59)	<b>1.80</b> (1.60-2.03)	<b>2.37</b> (2.11-2.67)	<b>2.84</b> (2.51-3.19)	<b>3.50</b> (3.08-3.92)	<b>4.03</b> (3.52-4.51)	<b>4.60</b> (3.99-5.15)	<b>5.20</b> (4.47-5.84)	<b>6.05</b> (5.14-6.79)	<b>6.74</b> (5.67-7.58)
7-day	<b>1.56</b> (1.39-1.76)	<b>1.99</b> (1.78-2.25)	<b>2.63</b> (2.34-2.97)	<b>3.15</b> (2.79-3.55)	<b>3.88</b> (3.42-4.36)	<b>4.47</b> (3.91-5.02)	<b>5.10</b> (4.43-5.73)	<b>5.76</b> (4.96-6.48)	<b>6.70</b> (5.70-7.54)	<b>7.46</b> (6.28-8.41)
10-day	<b>1.70</b> (1.51-1.91)	<b>2.17</b> (1.93-2.44)	<b>2.86</b> (2.54-3.22)	<b>3.42</b> (3.03-3.84)	<b>4.21</b> (3.70-4.71)	<b>4.83</b> (4.23-5.40)	<b>5.50</b> (4.78-6.15)	<b>6.20</b> (5.35-6.94)	<b>7.18</b> (6.12-8.05)	<b>7.97</b> (6.72-8.94)
20-day	<b>2.08</b> (1.86-2.33)	<b>2.68</b> (2.39-3.00)	<b>3.54</b> (3.16-3.95)	<b>4.19</b> (3.73-4.67)	<b>5.07</b> (4.48-5.65)	<b>5.74</b> (5.06-6.40)	<b>6.42</b> (5.64-7.17)	<b>7.12</b> (6.22-7.95)	<b>8.05</b> (6.97-9.02)	<b>8.77</b> (7.53-9.84)
30-day	<b>2.43</b> (2.17-2.73)	<b>3.13</b> (2.79-3.50)	<b>4.13</b> (3.67-4.61)	<b>4.88</b> (4.34-5.44)	<b>5.90</b> (5.21-6.57)	<b>6.68</b> (5.88-7.43)	<b>7.48</b> (6.55-8.32)	<b>8.29</b> (7.23-9.23)	<b>9.39</b> (8.12-10.5)	<b>10.2</b> (8.78-11.4)
45-day	<b>2.82</b> (2.52-3.15)	<b>3.63</b> (3.25-4.06)	<b>4.78</b> (4.28-5.34)	<b>5.64</b> (5.03-6.29)	<b>6.76</b> (6.01-7.54)	<b>7.61</b> (6.74-8.49)	<b>8.46</b> (7.47-9.45)	<b>9.32</b> (8.18-10.4)	<b>10.4</b> (9.11-11.7)	<b>11.3</b> (9.79-12.7)
60-day	<b>3.12</b> (2.80-3.48)	<b>4.03</b> (3.62-4.49)	<b>5.30</b> (4.75-5.90)	<b>6.22</b> (5.56-6.92)	<b>7.42</b> (6.62-8.26)	<b>8.31</b> (7.39-9.25)	<b>9.20</b> (8.15-10.2)	<b>10.1</b> (8.89-11.2)	<b>11.2</b> (9.84-12.5)	<b>12.1</b> (10.5-13.5)

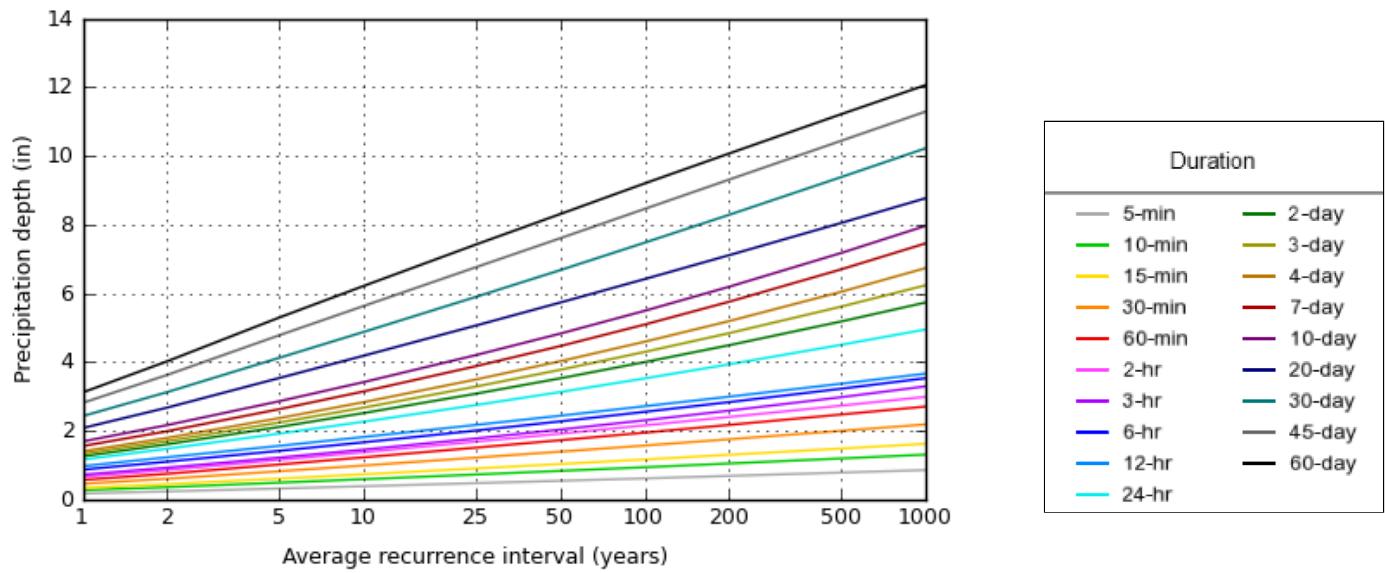
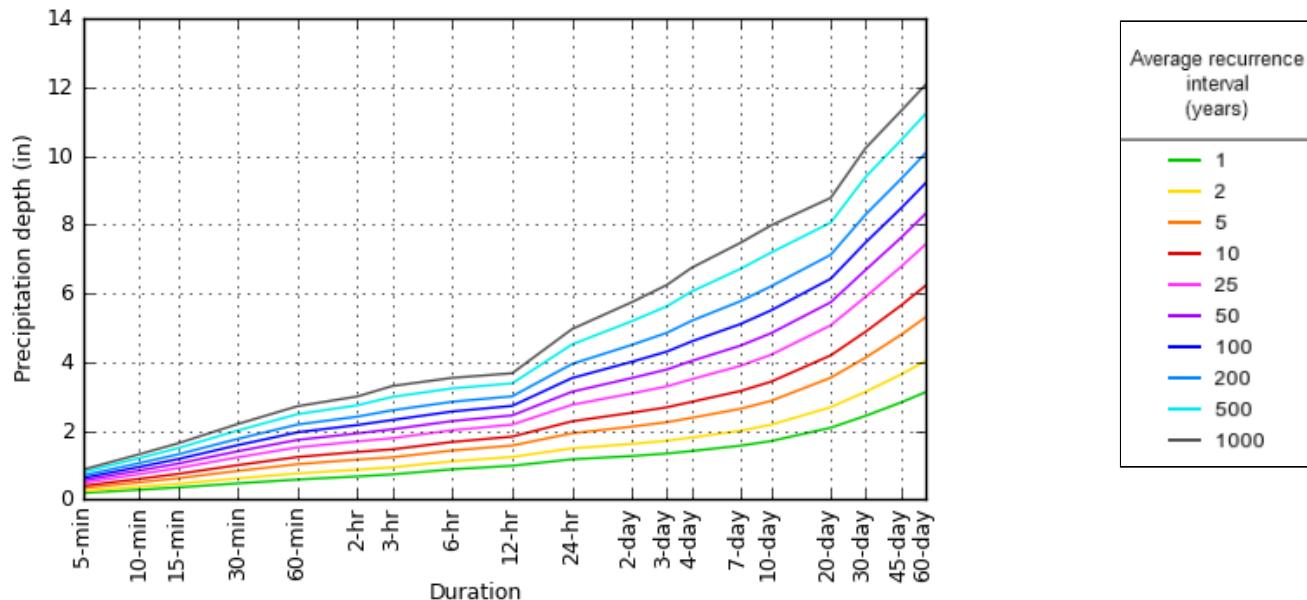
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)**PF graphical**

PDS-based depth-duration-frequency (DDF) curves  
Latitude: 33.4955°, Longitude: -111.9279°



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## Maps & aerials

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## NOAA Atlas 14, Volume 1, Version 5

Location name: Scottsdale, Arizona, USA\*

Latitude: 33.4955°, Longitude: -111.9279°

Elevation: 1262.91 ft\*\*

\* source: ESRI Maps

\*\* source: USGS



## POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)

## PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	2.20 (1.85-2.68)	2.88 (2.42-3.50)	3.91 (3.28-4.74)	4.70 (3.91-5.68)	5.77 (4.72-6.94)	6.60 (5.33-7.90)	7.44 (5.90-8.88)	8.32 (6.47-9.90)	9.47 (7.18-11.3)	10.3 (7.69-12.4)
10-min	1.67 (1.40-2.04)	2.19 (1.84-2.66)	2.98 (2.49-3.61)	3.58 (2.98-4.32)	4.40 (3.59-5.28)	5.03 (4.06-6.01)	5.66 (4.49-6.76)	6.32 (4.93-7.54)	7.20 (5.46-8.59)	7.87 (5.86-9.41)
15-min	1.38 (1.16-1.68)	1.81 (1.52-2.20)	2.46 (2.06-2.98)	2.96 (2.46-3.57)	3.63 (2.97-4.36)	4.15 (3.35-4.97)	4.68 (3.71-5.59)	5.23 (4.07-6.23)	5.95 (4.52-7.10)	6.51 (4.84-7.78)
30-min	0.930 (0.780-1.13)	1.22 (1.03-1.48)	1.65 (1.38-2.01)	1.99 (1.65-2.40)	2.45 (2.00-2.94)	2.80 (2.26-3.34)	3.15 (2.50-3.76)	3.52 (2.74-4.19)	4.01 (3.04-4.78)	4.38 (3.26-5.24)
60-min	0.576 (0.483-0.702)	0.754 (0.635-0.917)	1.02 (0.857-1.24)	1.23 (1.02-1.49)	1.51 (1.24-1.82)	1.73 (1.40-2.07)	1.95 (1.55-2.33)	2.18 (1.70-2.60)	2.48 (1.88-2.96)	2.71 (2.02-3.24)
2-hr	0.334 (0.284-0.398)	0.432 (0.368-0.517)	0.578 (0.492-0.688)	0.690 (0.580-0.820)	0.843 (0.700-0.994)	0.960 (0.786-1.13)	1.08 (0.872-1.27)	1.20 (0.953-1.41)	1.37 (1.06-1.61)	1.50 (1.13-1.77)
3-hr	0.242 (0.205-0.291)	0.310 (0.264-0.375)	0.408 (0.345-0.490)	0.485 (0.407-0.580)	0.593 (0.491-0.705)	0.679 (0.554-0.805)	0.769 (0.616-0.911)	0.863 (0.680-1.02)	0.993 (0.759-1.18)	1.10 (0.818-1.30)
6-hr	0.146 (0.126-0.172)	0.185 (0.161-0.218)	0.237 (0.205-0.278)	0.279 (0.239-0.325)	0.336 (0.284-0.389)	0.380 (0.317-0.440)	0.427 (0.350-0.493)	0.474 (0.381-0.549)	0.539 (0.423-0.625)	0.591 (0.452-0.687)
12-hr	0.081 (0.071-0.094)	0.103 (0.090-0.119)	0.130 (0.113-0.150)	0.151 (0.131-0.175)	0.181 (0.154-0.208)	0.203 (0.171-0.233)	0.226 (0.188-0.260)	0.249 (0.205-0.287)	0.280 (0.225-0.324)	0.305 (0.240-0.355)
24-hr	0.049 (0.043-0.055)	0.062 (0.055-0.070)	0.080 (0.071-0.090)	0.095 (0.084-0.106)	0.115 (0.101-0.129)	0.131 (0.114-0.146)	0.147 (0.128-0.165)	0.164 (0.142-0.184)	0.188 (0.160-0.211)	0.206 (0.174-0.232)
2-day	0.026 (0.023-0.030)	0.034 (0.030-0.038)	0.044 (0.039-0.050)	0.053 (0.047-0.059)	0.064 (0.057-0.072)	0.074 (0.065-0.083)	0.083 (0.073-0.094)	0.094 (0.081-0.105)	0.108 (0.092-0.122)	0.120 (0.101-0.135)
3-day	0.019 (0.017-0.021)	0.024 (0.021-0.027)	0.031 (0.028-0.035)	0.037 (0.033-0.042)	0.046 (0.040-0.051)	0.052 (0.046-0.059)	0.060 (0.052-0.067)	0.067 (0.058-0.076)	0.078 (0.067-0.088)	0.087 (0.073-0.098)
4-day	0.015 (0.013-0.017)	0.019 (0.017-0.021)	0.025 (0.022-0.028)	0.030 (0.026-0.033)	0.036 (0.032-0.041)	0.042 (0.037-0.047)	0.048 (0.042-0.054)	0.054 (0.047-0.061)	0.063 (0.054-0.071)	0.070 (0.059-0.079)
7-day	0.009 (0.008-0.010)	0.012 (0.011-0.013)	0.016 (0.014-0.018)	0.019 (0.017-0.021)	0.023 (0.020-0.026)	0.027 (0.023-0.030)	0.030 (0.026-0.034)	0.034 (0.030-0.039)	0.040 (0.034-0.045)	0.044 (0.037-0.050)
10-day	0.007 (0.006-0.008)	0.009 (0.008-0.010)	0.012 (0.011-0.013)	0.014 (0.013-0.016)	0.018 (0.015-0.020)	0.020 (0.018-0.023)	0.023 (0.020-0.026)	0.026 (0.022-0.029)	0.030 (0.025-0.034)	0.033 (0.028-0.037)
20-day	0.004 (0.004-0.005)	0.006 (0.005-0.006)	0.007 (0.007-0.008)	0.009 (0.008-0.010)	0.011 (0.009-0.012)	0.012 (0.011-0.013)	0.013 (0.012-0.015)	0.015 (0.013-0.017)	0.017 (0.015-0.019)	0.018 (0.016-0.020)
30-day	0.003 (0.003-0.004)	0.004 (0.004-0.005)	0.006 (0.005-0.006)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.010 (0.009-0.012)	0.012 (0.010-0.013)	0.013 (0.011-0.015)	0.014 (0.012-0.016)
45-day	0.003 (0.002-0.003)	0.003 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.010 (0.008-0.011)	0.010 (0.009-0.012)
60-day	0.002 (0.002-0.002)	0.003 (0.003-0.003)	0.004 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.008 (0.007-0.009)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

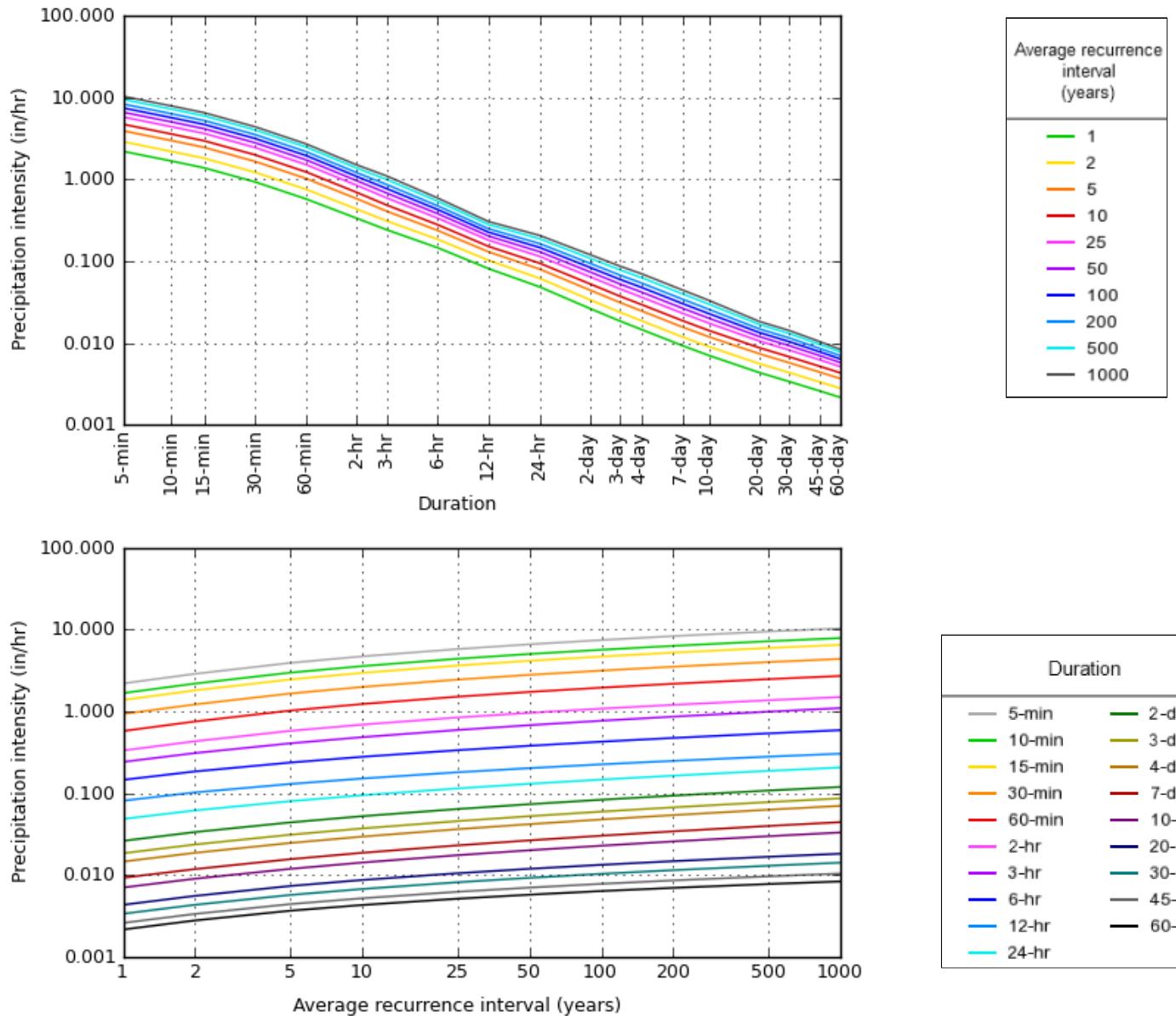
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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## PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 33.4955°, Longitude: -111.9279°



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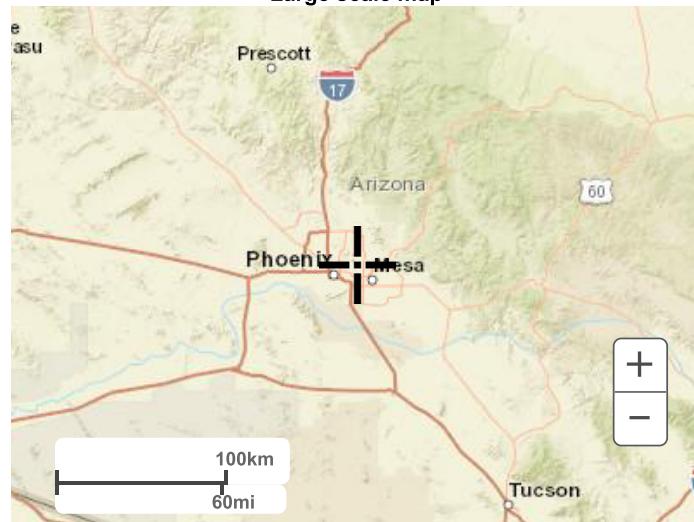
[Small scale terrain](#)



Large scale terrain



Large scale map



Large scale aerial

## *APPENDIX II*

### *Calculations*

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APPENDIX

10-ZN-2020

10/22/20

**Weighted Runoff Coefficient-Calculations (C<sub>w</sub>)**

PROPOSED OVERALL SITE C <sub>w</sub>					
	BUILDING or CONCRETE	ASPHALT	DESERT LANDSCAPE	TOTAL AREA	Cwt
C-VALUE	0.95	0.95	0.45		
AREA (ac)	2.46	0.65	0.07	3.18	<b>0.94</b>
DA-1	0.37	0.00	0.00	0.37	0.95
DA-2	0.19	0.26	0.02	0.47	0.93
DA-3	1.07	0.05	0.01	1.13	0.95
DA-4A	0.12	0.00	0.00	0.12	0.95
DA-4B	0.20	0.16	0.00	0.36	0.95
DA-5	0.42	0.00	0.04	0.46	0.91
DA-6	0.09	0.18	0.00	0.27	0.95

EXISTING OVERALL SITE C <sub>w</sub>					
	BUILDING or CONCRETE	ASPHALT	DESERT LANDSCAPE	TOTAL AREA	Cwt
C-VALUE	0.95	0.95	0.45		
AREA (ac)	1.66	1.34	0.18	3.18	<b>0.92</b>
EX-1	0.20	0.00	0.00	0.20	0.95
EX-2	0.67	0.00	0.00	0.67	0.95
EX-3	0.00	0.24	0.00	0.24	0.95
EX-4	0.00	0.36	0.00	0.36	0.95
EX-5A	0.12	0.00	0.00	0.12	0.95
EX-5B	0.35	0.00	0.01	0.36	0.94
EX-6	0.13	0.74	0.17	1.04	0.87
EX-7	0.19	0.00	0.00	0.19	0.95



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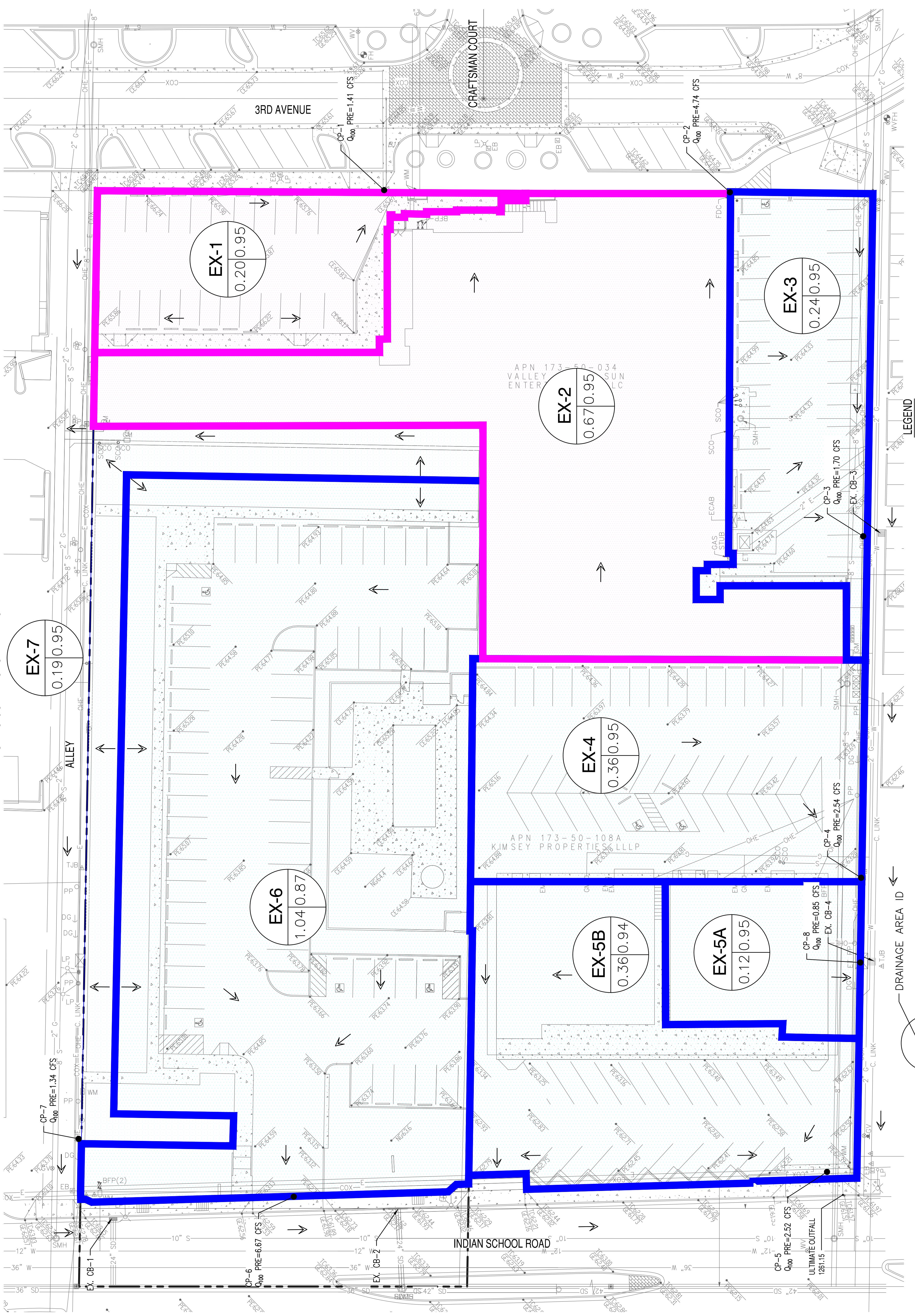
any

other



# THE TRIANGLE VENUE AND INDIAN SCHOOL ROAD CONDITIONS DRAINAGE AREA MAP

# 3RD AVENUE AND INDIAN SCHOOL ROAD EXISTING CONDITIONS DRAINAGE AREA MAP



## DRAINAGE AREA KEY

AREA IN ACRES \_\_\_\_\_ RUNOFF COEFFICIENT \_\_\_\_\_

DRAINAGE AREAS  
CONTRIBUTING TO INDIAN SCH.  
 FLOW ARROW

**EXISTING CONDITION  
DRAINAGE AREA MAP**

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SUSTAINABILITY  
ENGINEERING  
GROUP



8280 E. GEDDING DRIVE SUITE 101, SCOTTSDALE, ARIZONA 85260  
WWW.AZSEG.COM TEL: 480.588.7226 FAX: 480.259.3534



Call it least two full working days

for a 5-1-4 response

to a public records request

under A.R.S. § 36-3801 et seq.

Arizona State Seal

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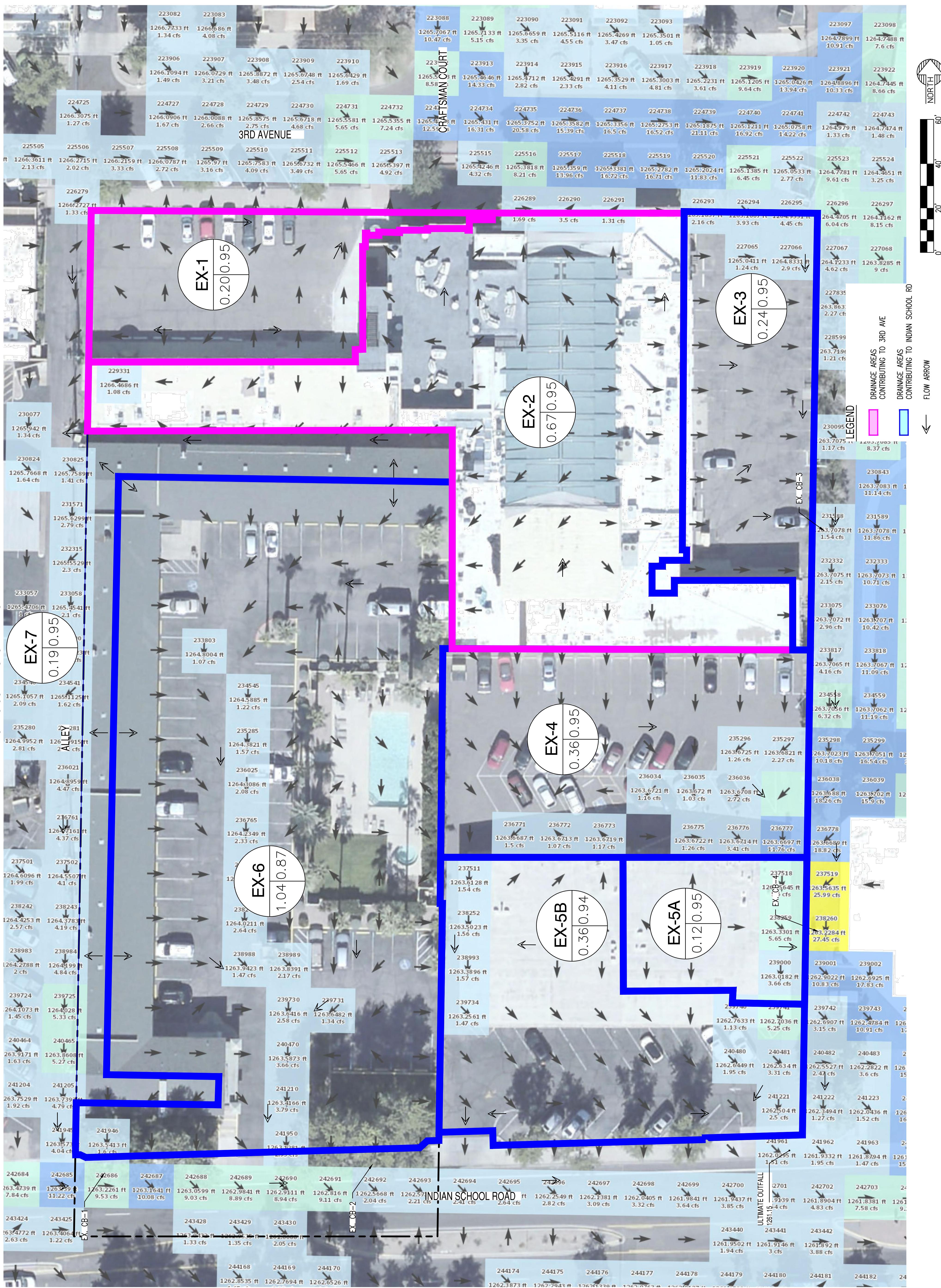
for a 5-1-4 response

to a public records request



# THE TRIANGLE LNU AND INDIAN SCHOOL ROAD CONDITIONS DRAINAGE AREA MAP

## **3RD AVENUE AND INDIAN SCHOOL ROAD EXISTING CONDITIONS DRAINAGE AREA MAP**



## **36" at S=0.0063 ft/ft; d/D=1.0**

---

### Project Description

---

Friction Method	Manning Formula
Solve For	Discharge

---

### Input Data

---

Roughness Coefficient	0.013
Channel Slope	0.006 ft/ft
Normal Depth	36.0 in
Diameter	36.0 in

---

### Results

---

Discharge	52.94 cfs
Flow Area	7.1 ft <sup>2</sup>
Wetted Perimeter	9.4 ft
Hydraulic Radius	9.0 in
Top Width	0.00 ft
Critical Depth	28.4 in
Percent Full	100.0 %
Critical Slope	0.007 ft/ft
Velocity	7.49 ft/s
Velocity Head	0.87 ft
Specific Energy	3.87 ft
Froude Number	(N/A)
Maximum Discharge	56.94 cfs
Discharge Full	52.94 cfs
Slope Full	0.006 ft/ft
Flow Type	Undefined

---

### GVF Input Data

---

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

---

### GVF Output Data

---

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	100.0 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	36.0 in
Critical Depth	28.4 in
Channel Slope	0.006 ft/ft
Critical Slope	0.007 ft/ft

---

## 48" at S=0.0063 ft/ft; d/D=1.0

### Project Description

Friction Method	Manning Formula
Solve For	Discharge

### Input Data

Roughness Coefficient	0.013
Channel Slope	0.006 ft/ft
Normal Depth	48.0 in
Diameter	48.0 in

### Results

Discharge	114.01 cfs
Flow Area	12.6 ft <sup>2</sup>
Wetted Perimeter	12.6 ft
Hydraulic Radius	12.0 in
Top Width	0.00 ft
Critical Depth	38.7 in
Percent Full	100.0 %
Critical Slope	0.007 ft/ft
Velocity	9.07 ft/s
Velocity Head	1.28 ft
Specific Energy	5.28 ft
Froude Number	(N/A)
Maximum Discharge	122.64 cfs
Discharge Full	114.01 cfs
Slope Full	0.006 ft/ft
Flow Type	Undefined

### GVF Input Data

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

### GVF Output Data

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	100.0 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	48.0 in
Critical Depth	38.7 in
Channel Slope	0.006 ft/ft
Critical Slope	0.007 ft/ft

## *APPENDIX III*

### *Preliminary Grading and Drainage Plans*

*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*



# THE TRIANGLE

7120 E INDIAN SCHOOL RD,  
SCOTTSDALE, AZ 85251

- CASE PRE-APP NUMBER -  
63-PA-2020

**PROFILE VIEW A-A**

SCALE: 1"=20'  
HORZ: 1"=20'  
VERT: 1"=2'

1270  
1268  
1266  
1264  
1262

-0+20 0+00 0+20 0+40 0+60 0+80 1+00 1+20 1+40 1+60 1+80 2+00 2+20 2+40 2+60 2+80

P  
R

BUILDING 1  
SIDEWALK  
PARKING  
1.9%  
17.65'  
20.1'

BUILDING 2  
TRASH ENCLOSURE  
20'  
DRIVE  
3.8%  
FFE=66.00

LANDSCAPE  
FFE=66.00  
EXISTING GROUND  
PROPOSED GRADE  
1.3%  
0.7%

1266  
1264  
1262

1262 1264 1266 1268 1270

**PROFILE E VIEW B-B**

SCALE: 1" = 20'

FFE = Footprint Edge

Building 2 FFE = 66.00

Building 5 FFE = 65.00

Building 6 FFE = 64.50

SIDEWALK 7.95'

INDIAN SCHOOL ROAD

PROPOSED GRADE

EXISTING GROUND

ROAD MAINTENANCE & P.U.E.

55' PROPOSED R.O.W.

' ROAD & P.U.E.

0+60 0+80 1+00 1+20 1+40 1+60 1+80 2+00 2+20 2+40 2+60 2+80 3+00

Detailed description: This is a site plan titled 'PROFILE E VIEW B-B'. It shows a grid-based layout with buildings, roads, and grade levels. Building 2 has an FFE of 66.00. Building 5 has an FFE of 65.00. Building 6 has an FFE of 64.50. A sidewalk is shown as 7.95' wide. The Indian School Road is a major street. A proposed road alignment is shown with a 1.9% grade. Existing ground levels are also indicated. A scale bar at the bottom right shows 1 inch equals 20 feet. The plan includes labels for 'ROAD MAINTENANCE & P.U.E.' and '55' PROPOSED R.O.W.'. A note at the bottom left says "' ROAD & P.U.E.'".

HOR  
VER

**NOT FOR CONSTRUCTION**

This profile view shows the elevation changes along a section labeled C-C. The vertical axis represents height above a reference level, with major grid lines every 2' and minor grid lines every 1'. The horizontal axis represents distance along the profile, with labels for each 20' interval from 0+00 to 4+40.

The profile shows several key features:

- EXISTING GROUND:** A solid black line representing the current terrain.
- PROPOSED GRADE:** A dashed black line representing the planned elevation changes.
- EX BUILDING:** A building located at approximately 1266 ft elevation.
- BUILDING 4:** A building located at approximately 1266 ft elevation.
- BUILDING 5:** A building located at approximately 1264 ft elevation.
- SIDEWALK:** A 4' wide proposed access easement.
- ALLEY:** A 10' wide proposed access easement.
- EXISTING TELEPHONE LINE EASEMENT:** A 5' wide existing utility easement.
- EXISTING ELECTRIC LINE EASEMENT:** A 6' wide existing utility easement.
- PROPOSED SEWER AND WATER EASEMENT:** An 8' wide proposed utility easement.
- EXISTING SEWER AND WATER EASEMENT:** An 8' wide existing utility easement.
- FFE:** Foundation Footings and Equipment.
- Project Name:** 3RD AVENUE + INDIAN SCHOOL ROAD - SCOTTSDALE, AZ
- Project Number:** 200504 (SEG)
- Description:** PRELIMINARY CROSS SECTION
- Scale:** As indicated
- SCALE:** HORIZONTAL: 1" = 20', VERTICAL: 1" = 2'

**PROFILE VIEW C-C**

©2015 Gensler

CIVIL ENGINEER. SEG 8280 E. GELDING DR, SUITE #101 SCOTTSDALE, AZ 85260 480-588-7226 ATTN: ALI FAKIH

DEVELOPER/OWNER. PEG/ COMPANIES 180 N. UNIVERSITY AVE SUITE 200, UT 84601 801-655-1998 ATTN: MATT KRAMBULE

ARCHITECT. GENSLER 2575 E. CAMELBACK RD SUITE 175, PHOENIX AZ 85016 602-253-4900 ATTN: JOHANNA COLLINS

THE TRIANGLE

7120 E. INDIAN SCHOOL ROAD SCOTTSDALE, AZ 85251

DEVELOPER/OWNER:

PEG / COMPANIES  
1180 N. UNIVERSITY AVE  
SUITE 200, UT 84601  
801-655-1998

ARCHITECT:

GENSLER  
2575 E. CAMELBACK  
SUITE 175, PHOENIX  
602-253-4900

ATTN: JOHANNA COLE

ATTN: MATT KRAMBULE

# THE TRIANGLE

7120 E INDIAN SCHOOL RD,  
SCOTTSDALE, AZ 85251

- CASE PRE-APP NUMBER -  
63-PA-2020

**Gensler**  
2575 E Camelback Road  
Suite 175  
Phoenix, AZ 85016  
United States  
Tel 602.523.4900  
Fax 602.523.4949

**SYDNOR**  
4806 N 78TH Place  
Scottsdale, AZ 85251  
United States

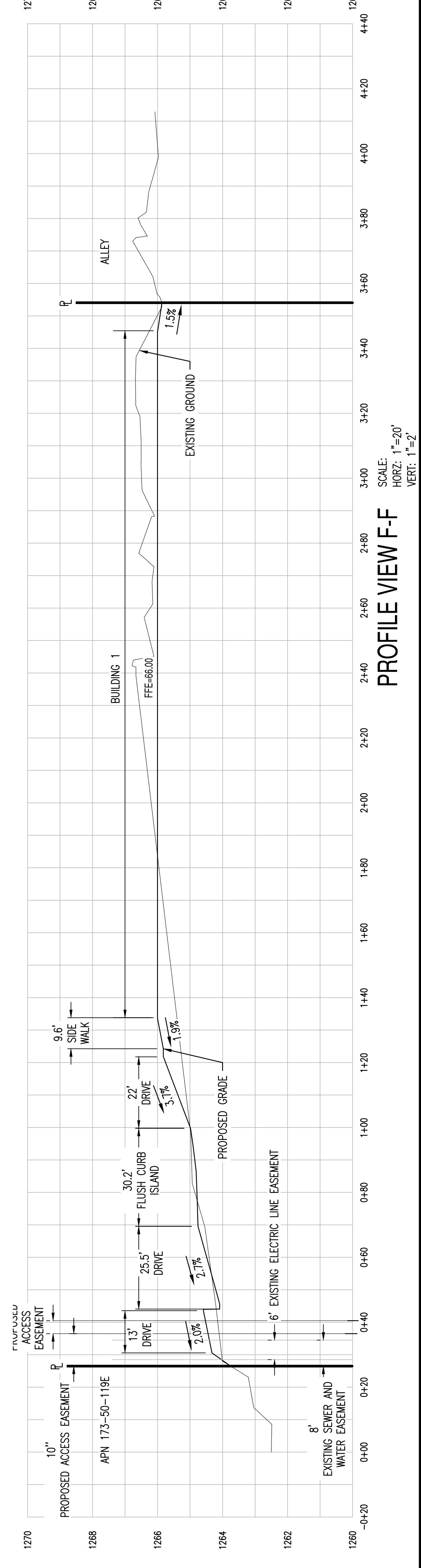
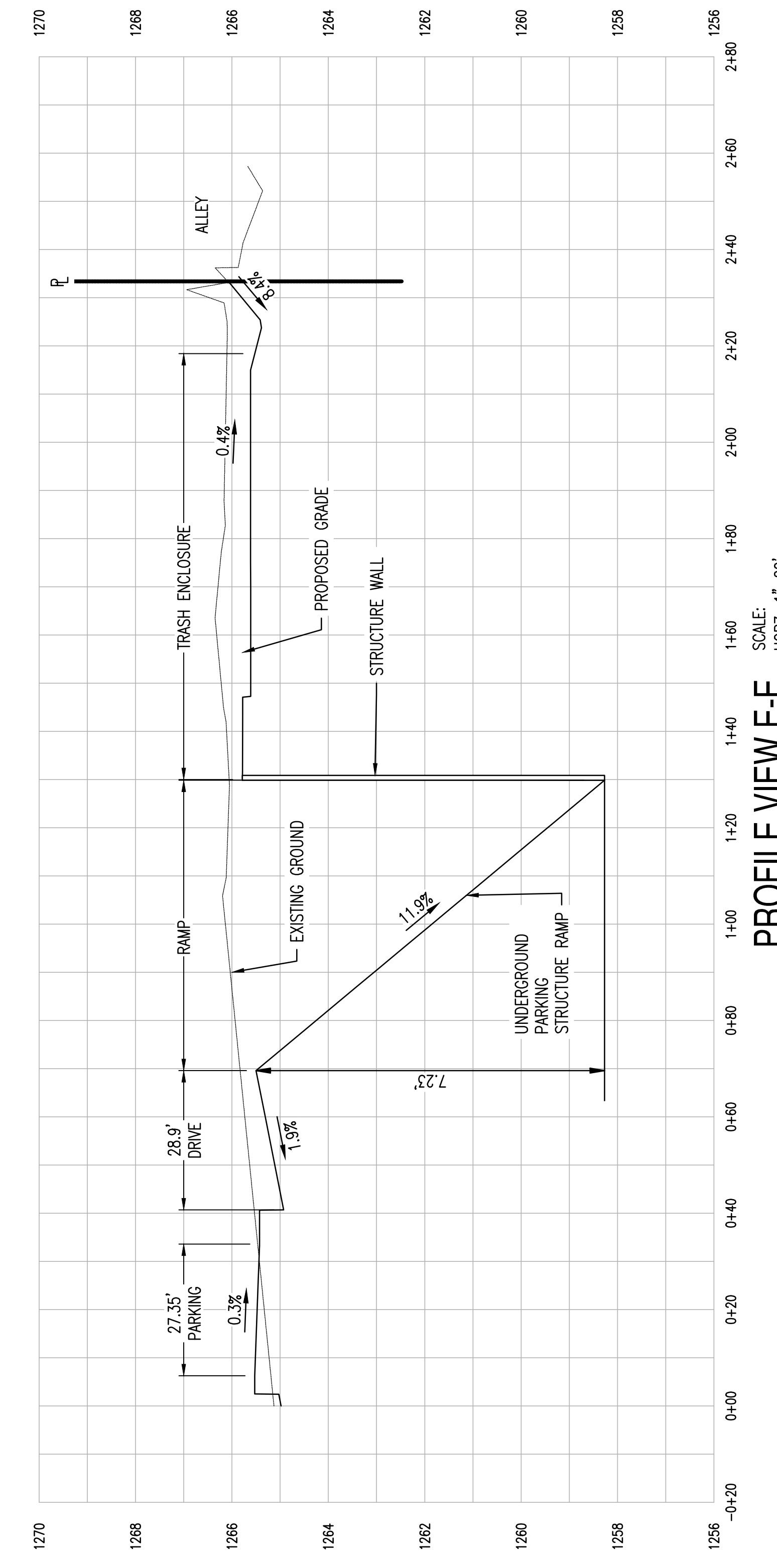
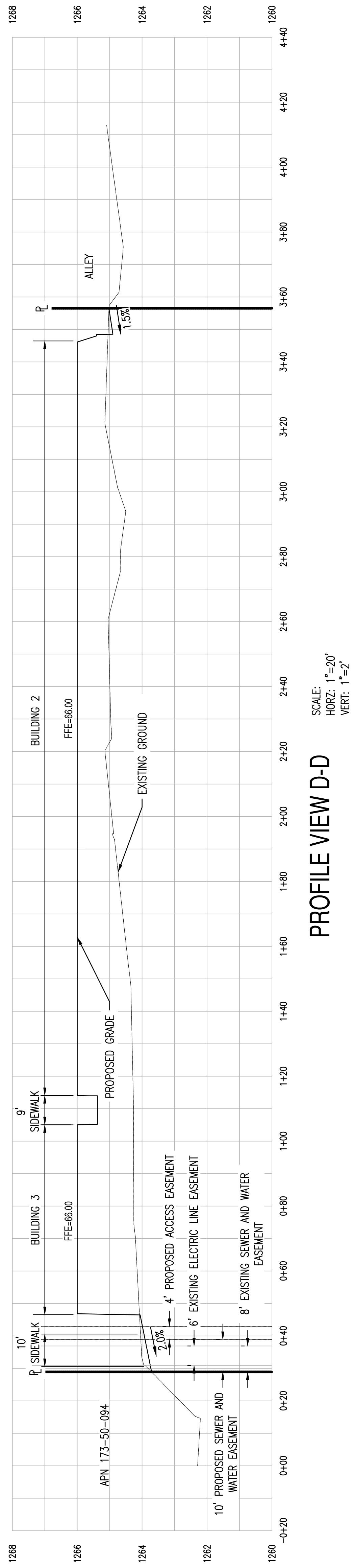
SEG  


8280 E. GELDING DRIVE  
Suite 101  
Scottsdale, AZ 85260  
United States  
Tel 480.588.7226

Seal / Signature	
<b>NOT FOR CONSTRUCTION</b>	
Project Name	3RD AVENUE+INDIAN SCHOOL ROAD - SCOTTSDALE, AZ
Project Number	200504 (SEG)
Description	PPEI IMINAPY CPOSS SECTION

As indicated

C3.51



## *APPENDIX IV*

### *Site Visit Photos*

*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*

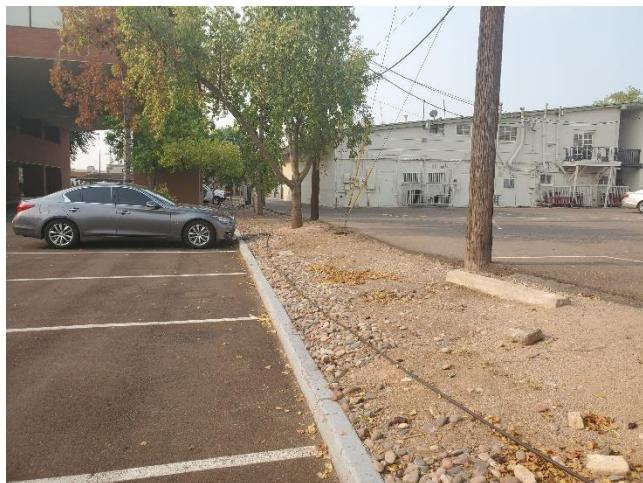
**EAST BOUNDARY SITE PHOTOS 8/27/2020**

NORTHEAST BOUNDARY OF PARCEL 173-50-119E

PARCEL 173-50-119E EXISTING INLET STRUCTURE, EX. CB-3



EAST BOUNDARY BETWEEN PARCELS 173-50-108A AND 173-50-094 LOOKING NORTH



EAST BOUNDARY BETWEEN PARCELS 173-50-108A AND 173-50-094 LOOKING SOUTH



SOUTHEAST BOUNDARY BETWEEN PARCELS  
173-50-108A AND 173-50-100A LOOKING NORTH

SOUTHEAST BOUNDARY BETWEEN THE TRIANGLE  
BUILDING AND PARCEL 173-50-100A LOOKING NORTH



SOUTHWEST CORNER OF PARCEL 173-50-100A



EXISTING INLET, EX. CB-4, IN PARCEL 173-50-100A

## *APPENDIX V*

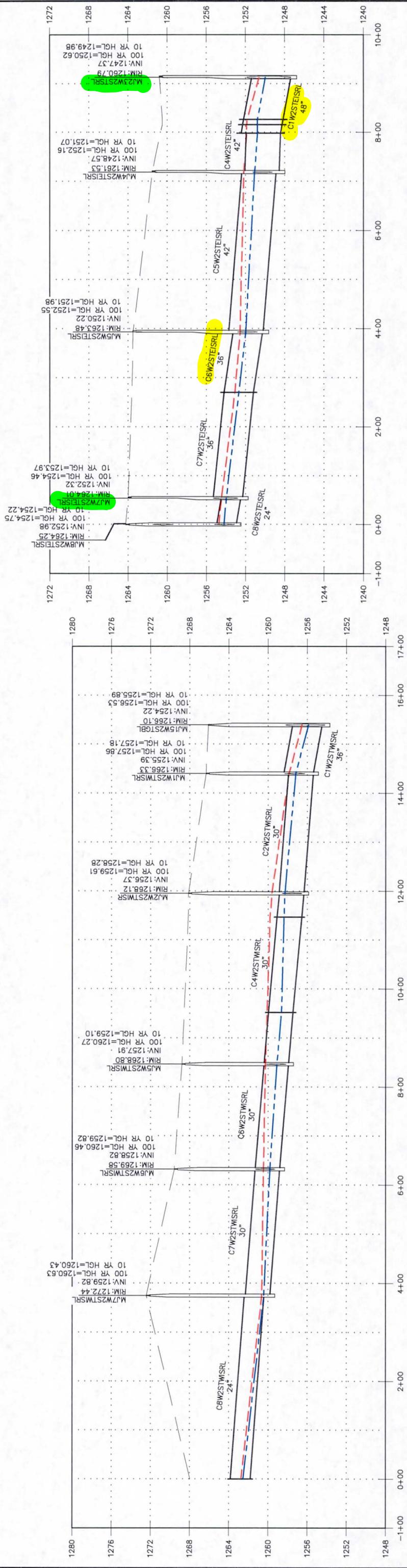
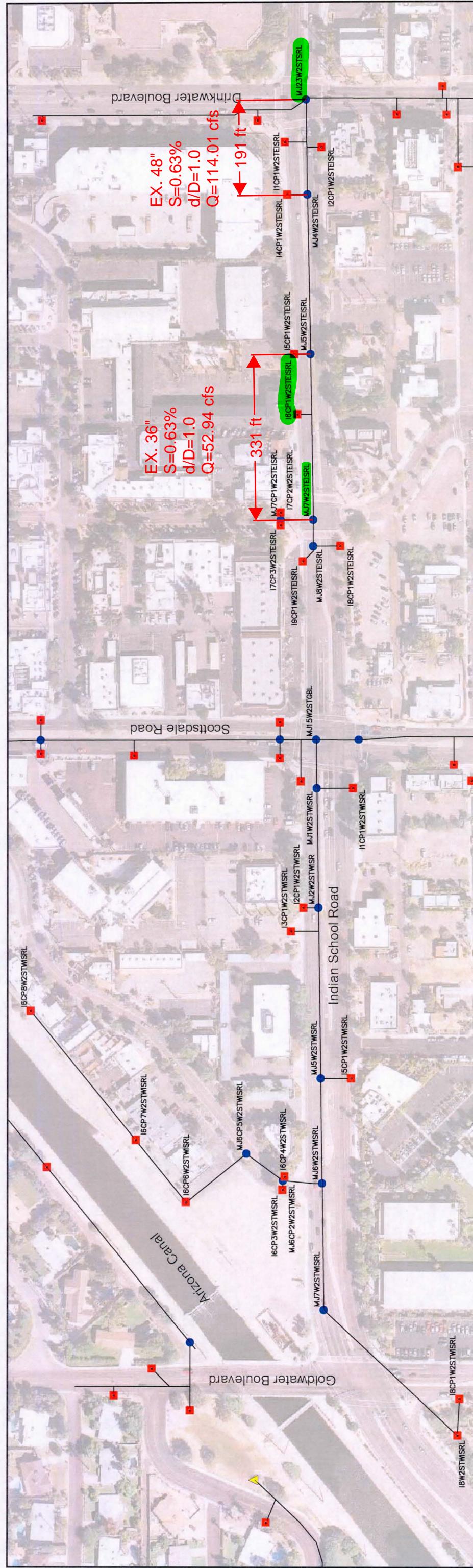
### *Lower Indian Bend Wash ADMP Excerpt*

*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*

Sustainability Engineering Group

[info@azSEG.com](mailto:info@azSEG.com) 480.588.7226 [www.azSEG.com](http://www.azSEG.com)

APPENDIX 10-ZN-2020  
10/22/20



SHEET SD29 OF SD121

SHEET SD29 OF SD SWMM Outfall:			
<b>W2STIBWOUTFALL</b>			
(West 2nd Street S.D. Outfall)			
Prepared	By	Checked	MIG
	AJA		12
			12

# LOWER INDIAN BEND WASH ADMSS/P STUDY AREA-SOUTH

Legend (Plan)	Legend (Profile)
Inlet & SWMM Identifier	— Ground Elevation
Manhole & SWMM Identifier	- - - Hydraulic Grade Line
Outlet & SWMM Identifier	— - - Hydraulic Grade Line
Storm Drain Pipes	— Storm Drain Pipes

Legend (Plan)
Inlet & SWMM Ident
Manhole & SWMM
Outlet & SWMM Id
Storm Drain Pipes

**Civil Engineering & Landscape Architecture**  
3030 North Glebe Avenue, Suite 1500  
P.O. Box 12177 • Fairfax, Virginia 22036-12177



Inlet Summary Table													
FLO-2D/SWMM Model													
SWMM Name	Curb High / Soffit High Inflow	100-yr, 24-hr				100-yr, 6-hr				10-yr, 24-hr			
		Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max		
Inlet	Connector Pipe	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		
I32CPM2ST	C32CPW2ST	14.4	0.5	0.5	0.5	0.3	0.4	0.4	0.4	0.4	0.4		
I32CP2W2ST	C32CP2W2ST	14.4	0.9	0.9	10	10	0.6	0.7	0.7	10.1	10.6		
I2CPM2STSRL	C2CPM2STSRL	7.2	4.9	4.9	5.4	3.4	4.0	4.0	4.0	13.1	13.0		
I1CPW2STSRL	C1CPW2STSRL	7.2	1.5	1.4	3.0	3.0	0.5	0.6	0.6	7.8	7.8		
I4CPW2STSRL	C4CPW2STSRL	7.2	5.6	5.6	6.4	2.5	3.5	3.5	3.5	2.0	2.0		
I6CPW2STSRL	C6CPW2STSRL	4.8	1.5	1.5	1.7	1.0	1.2	1.2	1.2	14.9	14.9		
I7CPW2STSRL	C7CPW2STSRL	9.6	7.3	7.3	8.6	4.0	5.1	5.1	5.1	7.0	7.0		
I8CPW2STSRL	C8CPW2STSRL	4.8	0.7	0.7	0.8	10	0.4	0.5	0.5	2.3	2.3		
I9CPW2STSRL	C9CPW2STSRL	4.8	0.9	0.9	18	0.6	0.6	0.7	0.7	8.5	8.5		
I5CP2W2STSRL	C5CP2W2STSRL	9.6	6.7	6.7	8.1	3.8	4.7	4.7	4.7	10.9	10.8		
I5CP3W2STSRL	C5CP3W2STSRL	14.4	14.8	14.7	15.6	11.4	12.7	12.7	12.7	7.2	7.2		
I21CPW2STSRL	C21CPW2STSRL	12.0	4.7	4.6	5.9	5.8	2.7	3.3	3.3	9.1	10.6		
I20CPW2STSRL	C20CPW2STSRL	12.0	2.7	2.7	4.0	4.0	1.5	1.8	1.8	9.2	10.6		
I15CPW2STSRL	C15CPW2STSRL	12.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	10	10		
I17CPW2STSRL	C17CPW2STSRL	4.8	1.1	1.1	13	0.6	0.6	0.7	0.7	4.6	4.6		
I16CPW2STSRL	C16CPW2STSRL	4.8	1.9	1.9	2.2	0.9	0.9	1.1	1.1	4.0	4.0		
I15CPW2STSRL	C15CPW2STSRL	4.8	4.0	4.0	4.2	2.9	2.9	3.3	3.3	10	10		
I14CPW2STSRL	C14CPW2STSRL	4.8	2.0	2.0	3.0	0.3	0.3	0.4	0.4	13	13		
I13CPW2STSRL	C13CPW2STSRL	7.2	3.3	3.2	3.8	3.8	16	15	2.0	2.0	2.0		
I10CP2W2STSRL	C10CP2W2STSRL	12.0	13.8	13.8	15.0	15.0	6.7	6.7	9.2	17	17		
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I12CPW2STSRL	C12CPW2STSRL	12.0	16	15	2.1	2.0	0.7	0.7	0.9	0.7	0.7		
I18CP2W2STSRL	C18CP2W2STSRL	14.4	8.4	8.3	9.9	9.8	5.3	5.3	6.2	7.3	7.3		
I18CPW2STSRL	C18CPW2STSRL	8.7	1.1	9.4	14	11.2	0.5	0.5	0.6	6.0	6.0		
I20CPW2ST	C20CPW2ST	32.2	11	11	2.0	2.3	0.3	0.3	0.5	12	12		
I21CPW2ST	C21CPW2ST	32.2	9.7	9.7	14.5	14.5	3.5	3.5	5.3	3.5	3.5		
I20CP2W2ST	C20CP2W2ST	32.2	0.8	0.8	16	0.3	0.3	0.4	0.4	9.1	9.1		
I1WZSTBAL	C1WZSTBAL	32.2	119	29.0	16.8	34.7	5.5	20.9	7.3	7.5	8.1		
I24CPW2ST	C24CPW2ST	2.6	16	16	2.0	2.0	10	10	12	15	15		
I24CP4W2ST	C24CP4W2ST	2.6	19	19	2.3	2.2	11	11	14	18	18		
I33CPW2ST	C33CPW2ST	20.0	15	15	19	19	0.9	0.9	1.1	6.4	6.4		
I34CPW2ST	C34CPW2ST	20.0	13	12	16	16	0.7	0.7	0.9	4.3	4.3		
I35CPW2ST	C35CPW2ST	20.0	18	18	2.3	2.3	10	10	12	3.8	3.8		
I37CPW2ST	C37CPW2ST	32.2	8.9	8.9	10.4	10.4	5.8	5.8	7.0	5.0	5.0		
I37CP2W2ST	C37CP2W2ST	32.2	3.0	3.0	3.6	3.6	18	18	2.2	3.7	3.6		
I36CPW2ST	C36CPW2ST	20.0	8.7	8.7	10.6	10.6	4.7	4.7	6.1	5.8	5.8		
I43CPW2ST	C43CPW2ST	32.2	110	110	13.2	13.1	5.5	5.5	6.7	4.1	4.1		
I47CPW2ST	C47CPW2ST	32.2	5.8	5.8	6.7	6.7	3.7	3.7	4.5	8.4	8.4		
I46CPW2ST	C46CPW2ST	7.4	16	16	2.0	2.0	0.8	0.8	1.1	3.8	3.8		
I2CPW2STSRL	C2CPW2STSRL	2.6	0.9	0.9	10	0.5	0.5	0.6	0.6	3.1	3.1		
I1CPW2STSRL	C1CPW2STSRL	2.6	3.1	3.1	3.2	3.2	1.7	1.7	2.0	3.5	3.5		
I9CPW2STSRL	C9CPW2STSRL	2.6	18	3.9	3.2	6.2	19	3.7	4.0	4.7	4.7		
I9CPW2STSRL	C9CPW2STSRL	2.6	1.9	2.0	3.1	3.0	2.0	2.2	2.2	5.0	5.0		
I7CPW2STSRL	C7CPW2STSRL	2.6	2.0	1.9	2.6	2.5	4.3	4.3	5.1	10.1	10.1		
I4CPW2STSRL	C4CPW2STSRL	3.6	5.5	5.4	5.9	5.4	5.3	5.3	5.3	15	15		

INLET SUMMARY TABLE NOTES:

- The curb high/soffit high inflow discharge were calculated according to the procedures outlined in the District's Hydraulics Manual.
- The peak hydrograph discharge taken from the 'Link Results' in the SWMM.RTP file.
- The pipe Max Discharge is the peak hydrograph discharge taken from the 'Link Results' in the SWMM.RTP file.

SHEET SD30 OF SD121



Gayan & Barker  
TYLIN INTERNATIONAL  
engineers | planners | scientists

City Engineering & Landscaping Architecture  
303 North Central Avenue, Suite 1500  
Phoenix, AZ 85004-3031  
480.992.0000

Prepared By AIA  
Checked MITG  
Date 12/18/2017  
2nd Street S.D. Outfall

Inlet Summary Table													
FLO-2D/SWMM Model													
SWMM Name	Curb High / Soffit High Inflow	100-yr, 24-hr				100-yr, 6-hr				10-yr, 24-hr			
		Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max	Inflow	Pipe Max		
Inlet	Connector Pipe	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		
I2CPW2STSRL	C2CPW2STSRL	7.4	0.5	0.5	0.3	0.3	0.4	0.4	0.4	7.9	10.5		
I1CPW2STSRL	C1CPW2STSRL	7.2	4.9	5.4	3.4	3.4	4.0	4.0	4.0	7.2	7.5		
I4CPW2STSRL	C4CPW2STSRL	7.2	1.5	1.4	3.0	0.5	0.6	0.6	0.6	7.8	7.8		
I6CPW2STSRL	C6CPW2STSRL	4.8	1.5	1.5	1.7	10	12	12	12	14.9	14.9		
I7CPW2STSRL	C7CPW2STSRL	7.2	1.2	1.2	1.7	1.0	1.2	1.2	1.2	7.0	7.0		
I8CPW2STSRL	C8CPW2STSRL	4.8	0.7	0.									

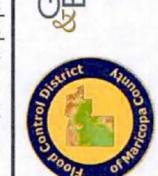
Inlet Summary Table

SWMM Name	FLO-2D/SWMM Model					
	100-yr, 24-hr		10-yr, 6-hr		10-yr, 6-hr	
	Curb High / Soffit High Inflow (cfs)	Pipe Max Inflow (cfs)				
I19CP2W2STGBL	C19CP2W2STGBL	7.0	4.3	4.9	2.8	2.7
I20CP7W2STGBL	C20CP7W2STGBL	5.0	0.7	0.8	0.4	0.5
I20CP7W2STGBL	C20CP7W2STGBL	7.0	0.3	0.3	0.2	0.2
I20CP9W2STGBL	C20CP9W2STGBL	7.0	59	6.9	3.8	4.6
I20CP4W2STGBL	C20CP4W2STGBL	7.0	5.2	58	3.6	4.2
I20CP5W2STGBL	C20CP5W2STGBL	7.0	2.0	2.5	12	14
I20CP2W2STGBL	C20CP2W2STGBL	5.0	13	15	0.7	0.8
I8CP2W2STBAL	C8CP2W2STBAL	3.1	10	11	0.7	1.0
I29CPW2STSRL	C29CPW2STSRL	113	112	12.4	8.6	9.6
I7CPW2ST	C7CPW2ST	3.4	15	17	1.1	1.2
I9CPW2ST	C9CPW2ST	3.4	2.7	2.9	2.1	2.3
I6ACPW2ST	C6ACPW2ST	5.2	10.2	10.8	10.9	8.6
I5CPW2STCCL	C5CPW2STCCL	10.8	0.6	0.6	0.7	0.4
I8CPW2STCCL	C8CPW2STCCL	2.5	2.5	2.9	16	19
I4CP3W2STCCL	C4CP3W2STCCL	2.5	2.3	2.8	13	16
I4CP2W2STCCL	C4CP2W2STCCL	2.5	0.1	0.1	0.1	0.1
I1CPW2STCCL	C11CPW2STCCL	2.5	0.4	11	0.5	0.3
I1CP2W2STCCL	C11CP2W2STCCL	2.5	0.7	0.7	0.9	0.5
I1CP3W2STCCL	C11CP3W2STCCL	2.5	0.5	2.0	2.4	0.3
I1CP4W2STCCL	C11CP4W2STCCL	2.5	16	19	19	0.9
I10CPW2STCCL	C10CPW2STCCL	2.5	0.9	0.9	10	0.5
I9CPW2STCCL	C9CPW2STCCL	2.5	14	14	17	0.9
I6CPW2STCCL	C6CPW2STCCL	10.8	0.4	0.4	0.5	0.2
I7CPW2STCCL	C7CPW2STCCL	2.5	16	16	2.0	0.8
I2CPW2STBAL	C2CPW2STBAL	4.4	3.0	3.0	3.3	2.4
I2CPW2STBAL	C2CPW2STBAL	2.6	18	4.8	2.1	5.4
I37ACP2W2ST	C37ACP2W2ST	2.6	3.3	3.3	3.7	2.6
I0ACPW2ST	C10ACPW2ST	3.5	3.0	3.0	3.3	2.4
I0ACP2W2ST	C10ACP2W2ST	3.6	18	18	2.0	2.0
I3CP5W2STDPL	C3CP5W2STDPL	7.0	111	110	117	5.9
I3CP4W2STDPL	C3CP4W2STDPL	11.0	8.5	32.3	17.9	38.2
I3CP6W2STDPL	C3CP6W2STDPL	17.0	14.7	14.2	14.8	14.0
I3CP2W2STDPL	C3CP2W2STDPL	17.0	9.2	9.1	10.0	9.7
I3CPW2STDPL	C3CPW2STDPL	20.4	2.4	19.4	6.1	22.4
I3CP3W2STDPL	C3CP3W2STDPL	17.0	8.5	8.5	9.3	9.9
I2BGPW2ST	C12BGPW2ST	4.7	0.3	0.3	0.4	13
I1BGP2W2ST	C11BGP2W2ST	31.4	4.3	4.3	50	4.9
I1BGPW2ST	C11BGPW2ST	19.5	2.4	6.7	3.0	7.8
I11ACPW2ST	C11ACPW2ST	3.6	0.5	0.5	0.6	0.6
I12BGP2W2ST	C12BGP2W2ST	3.5	0.9	0.9	10	12
I11BGP4W2ST	C11BGP4W2ST	7.6	8.8	8.8	10.3	10.1
I11BGP5W2ST	C11BGP5W2ST	7.8	5.5	5.5	6.8	6.6
I19BGP2W2ST	C19BGP2W2ST	3.5	2.5	2.5	2.9	16
I19BGPW2ST	C19BGPW2ST	3.2	19	4.3	2.4	53
I19ACPW2ST	C19ACPW2ST	3.4	13	13	17	16

INLET SUMMARY TABLE NOTES:

- The curb high/soffit high inflow discharge were calculated according to the procedures outlined in the District's Hydraulics Manual.
- The inflow hydrograph discharge taken from the SWMMQIN.OUT file.
- The pipe Max Discharge is the peak hydrograph discharge taken from the 'Link Results' in the SWMM.RTP file.

## LOWER INDIAN BEND WASH ADMSS/P STUDY AREA-SOUTH



SWMM Outfall: W2STIBWOUFFALL (West 2nd Street S.D. Outfall)	
Prepared By AIA MTG	Date 12/18/2017 12/18/2017

SHEET SD31 OF SD121

Pipe Discharge Summary Table									
Conduit Name	FLO-2D/SWMM Model Discharge			FLO-2D/SWMM Model Discharge			FLO-2D/SWMM Model Discharge		
	Normal Depth Capacity (cfs)	100-yr, 24-hr (cfs)	100-yr, 6-hr (cfs)	Conduit Name	Normal Depth Capacity (cfs)	100-yr, 24-hr (cfs)	100-yr, 6-hr (cfs)	Conduit Name	Normal Depth Capacity (cfs)
C1W2ST	246.4	485.0	550.2	272.7	334.0	C37BW2ST	485.6	'60.5	189.3
C2W2ST	337.3	484.5	549.8	272.2	334.2	C38BW2ST	322.2	149.6	175.5
C3W2ST	329.8	482.8	549.8	274.1	335.0	C39BW2ST	52.8	148.7	174.5
C4W2ST	344.7	484.4	549.9	272.4	331.1	C40BW2ST	62.72	148.3	174.1
C5W2ST	270.9	484.4	549.7	271.6	330.1	C41BW2ST	2016	214	25.1
C6AW2ST	277.9	480.7	545.2	270.2	328.2	C42BW2ST	96.8	215	25.2
C6BW2ST	272.4	470.3	534.2	263.4	320.3	C43BW2ST	59.5	215	25.2
C7W2ST	235.5	470.3	534.2	278.9	319.9	C44BW2ST	77.0	10.8	12.4
C8W2ST	254.7	468.9	533.0	270.1	322.5	C45BW2ST	79.4	10.9	12.6
C9W2ST	204.0	468.9	533.0	271.5	325.6	C1W2STGBL	63.57	127.1	149.3
C10AW2ST	229.5	466.4	530.2	271.6	326.3	C2W2STGBL	108.3	127.0	149.2
C10BW2ST	288.4	462.3	525.6	271.4	335.3	C3W2STGBL	109.4	123.0	144.0
C11AW2ST	240.9	462.2	525.8	263.9	321.4	C4W2STGBL	108.8	115.9	135.4
C11BW2ST	283.6	462.1	525.6	269.4	320.1	C5W2STGBL	109.0	107.0	125.9
C12AW2ST	274.9	449.6	512.3	258.7	322.8	C6W2STGBL	87.9	10.10	18.8
C12BW2ST	288.4	449.5	512.0	259.2	348.3	C7W2STGBL	108.0	99.3	16.8
C12CW2ST	282.7	449.2	511.8	258.6	346.4	C8W2STGBL	110.6	91.6	108.1
C13W2ST	204.0	449.2	512.0	263.4	319.0	C9W2STGBL	111.5	91.6	107.8
C14N2ST	228.7	448.9	511.8	265.5	319.2	C10W2STGBL	1110	88.4	103.1
C15AW2ST	268.7	449.0	511.6	260.5	313.6	C11W2STGBL	112.5	78.7	91.9
C15BW2ST	243.8	402.9	449.7	243.2	284.9	C12W2STGBL	111.5	70.5	82.2
C16W2ST	257.1	402.8	449.6	245.6	284.2	C13W2STGBL	111.1	70.7	82.5
C17W2ST	987.1	402.8	449.7	253.3	284.3	C14W2STGBL	111.1	70.8	82.7
C18W2ST	868.0	394.9	442.9	248.7	282.9	C15W2STGBL	172.5	70.9	82.8
C19AW2ST	976.5	394.8	442.9	246.7	297.6	C16W2STGBL	262.7	36.5	43.3
C19BW2ST	941.6	393.8	441.7	245.4	301.5	C17W2STGBL	262.2	32.6	39.0
C19CW2ST	938.8	389.9	437.0	242.8	296.4	C18W2STGBL	61.9	25.7	30.5
C20W2ST	948.6	387.2	437.0	236.4	295.8	C19W2STGBL	61.9	22.3	26.0
C21W2ST	946.1	389.8	433.3	235.3	291.6	C20W2STGBL	36.5	15.6	18.2
C22W2ST	644.9	342.3	386.7	203.9	260.7	C21W2STGBL	7.8	0.4	0.5
C23N2ST	353.3	345.3	386.4	217.8	2912	C23W2STGBL	2055.1	173.8	195.6
C24N2ST	494.4	351.9	386.6	205.6	255.5	C24W2STGBL	790.3	172.7	205.7
C25W2ST	486.3	345.0	383.0	206.3	253.9	C25W2STGBL	1925.0	168.3	193.4
C26W2ST	508.6	345.4	385.0	208.8	254.0	C24W2STSRL	64.5	168.3	197.4
C27W2ST	510.7	345.8	388.5	207.4	252.7	C25W2STSRL	164.1	163.4	191.2
C28W2ST	512.4	347.4	390.9	206.0	251.5	C26W2STSRL	163.6	142.2	168.0
C29W2ST	156.1	349.7	391.6	206.4	251.2	C27W2STSRL	100.9	140.9	166.6
C30W2ST	275.1	176.9	196.5	105.3	128.2	C28W2STSRL	163.9	134.0	158.3
C31W2ST	266.9	177.0	196.7	105.5	128.3	C29W2STSRL	167.5	133.2	157.5
C32W2ST	276.6	176.9	196.9	105.6	128.3	C30W2STSRL	164.0	132.1	155.4
C33W2ST	273.5	176.3	195.9	105.3	127.9	C31W2STSRL	154.1	16.8	137.2
C34W2ST	133.9	175.1	194.8	104.7	127.3	C32W2STSRL	98.3	16.8	137.1
C35W2ST	272.8	174.1	194.2	104.2	126.9	C33W2STSRL	139.6	115.5	135.5
C36W2ST	423.5	172.6	193.6	103.6	125.9	C34W2STSRL	76.2	112.5	131.9
C37AW2ST	413.9	164.4	195.2	99.3	119.9	C35W2STSRL	139.4	110.7	129.2

PIPE DISCHARGE SUMMARY TABLE NOTES:

- The normal depth capacity discharges were obtained from the SWMM.RPT file.
- The pipe discharge is the peak hydrograph discharge taken from the "Link Results" in the SWMM.RTP file.

1. The normal depth capacity discharges were obtained from the SWMM.RPT file.  
2. The pipe discharge is the peak hydrograph discharge taken from the 'Link Results' in the SWMM.RTP file.

Pipe Discharge Summary Table

Pipe Discharge Summary Table									
Conduit Name	FLO-2D/SWMM Model Discharge			FLO-2D/SWMM Model Discharge			FLO-2D/SWMM Model Discharge		
	Normal Depth Capacity (cfs)	100-yr, 24-hr (cfs)	100-yr, 6-hr (cfs)	Conduit Name	Normal Depth Capacity (cfs)	100-yr, 24-hr (cfs)	100-yr, 6-hr (cfs)	Conduit Name	Normal Depth Capacity (cfs)
C16W2ST	106.7	124.8	106.7	C16W2STSRL	138.7	104.9	122.5	C17W2STSRL	139.7
C17W2ST	103.9	121.3	103.9	C18W2STSRL	139.3	105.5	121.3	C19W2STSRL	136.9
C19W2ST	111.1	111.1	111.1	C19W2STSRL	111.1	111.1	111.1	C20W2STSRL	87.9
C20W2ST	110.9	110.9	110.9	C20W2STSRL	87.9	95.3	110.9	C21W2STSRL	92.8
C21W2ST	107.3	107.3	107.3	C21W2STSRL	107.3	92.8	107.3	C22W2STSRL	135.5
C22W2ST	105.5	105.5	105.5	C22W2STSRL	135.5	92.8	105.5	C23W2STSRL	88.2
C23W2ST	104.9	104.9	104.9	C23W2STSRL	104.9	95.3	104.9	C24W2STSRL	89.1

Pipe Discharge Summary Table

Pipe Discharge Summary Table									
Conduit Name	FLO-2D/SWMM Model Discharge								
<th colspan="3

## *APPENDIX VI*

### *Stormwater Storage Waiver*

*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*

Sustainability Engineering Group

[info@azSEG.com](mailto:info@azSEG.com) 480.588.7226 [www.azSEG.com](http://www.azSEG.com)

APPENDIX 10-ZN-2020  
10/22/20

# Request for Stormwater Storage Waiver



## City of Scottsdale Plan/Case Numbers:

10-ZN-2020 - DR - \_\_\_\_\_ - PP - \_\_\_\_\_ PC# \_\_\_\_\_

Requests for stormwater storage waivers are reviewed as part of case submittals for the associated project. This form should be included in the preliminary drainage report with the applicant's portion completed. The preliminary drainage report shall include supporting documentation and analysis as needed to support the requested waiver.

Date \_\_\_\_\_ Project Name \_\_\_\_\_

Project Location \_\_\_\_\_

Applicant Contact \_\_\_\_\_ Company Name \_\_\_\_\_

Phone \_\_\_\_\_ E-mail \_\_\_\_\_

Address \_\_\_\_\_

### Waiver Criteria

A project must meet at least one of three criteria listed below for the city to consider waiving some or all required stormwater storage. **However, regardless of the criteria, a waiver will only be granted if the applicant can demonstrate that the effect of a waiver will not increase the potential for flooding on any property.** Check the applicable box and provide a signed and sealed engineering report and supporting engineering analysis that demonstrate the project meets the criteria and that the effect of a waiver will not increase the potential for flooding on any property.

If the runoff for the project has been included in a storage facility at another location, the applicant must demonstrate that the stormwater storage facility was specifically designed to accommodate runoff from the subject property and that the runoff will be conveyed to this location through an adequately designed conveyance facility.

It should be noted that reductions in stormwater storage relating to

- 1. The development is adjacent to a conveyance facility that an engineering analysis shows is designed and constructed to handle the additional runoff from the site as a result of development.
- 2. The development is on a parcel less than one-half acre in size.
- 3. Stormwater storage requirements conflict with requirements of the Environmentally Sensitive Lands Ordinance (ESLO).

For a full storage waiver, a conflict with ESLO is limited to:

- Property located in the hillside landform as defined in the city Zoning Ordinance
- Property in the upper desert landform that has a land slope steeper than 5% as defined in the city Zoning Ordinance
- Property within the ESL zoning overlay district where the only viable location for a stormwater storage basin requires blasting

This full waiver only applies to those portions of property meeting one of these three requirements.

100-year/2-hour storage is allowed, but not required for redevelopment projects and development within the ESL zoning overlay. Rather, these projects must store enough stormwater to attenuate post-development flows to predevelopment levels, considering the 10- and 100-year storm events (S.R.C. Sections 37-50 and 37-51).

By signing below, I certify that the stated project meets the waiver criteria selected above as demonstrated by the attached documentation.

## Stormwater Management Department

7447 E Indian School Road, Suite 125, Scottsdale, AZ 85251 • Phone: 480-312-2500

# Request for Stormwater Storage Waiver



10-ZN-2020

**City of Scottsdale Plan/Case Numbers:**

- DR - \_\_\_\_\_

- PP - \_\_\_\_\_

PC# \_\_\_\_\_

## **CITY STAFF TO COMPLETE THIS PAGE**

Project Name \_\_\_\_\_

### **Check Appropriate Boxes:**

- Meets waiver criteria (specify):  1     2     3

#### Recommended Conditions of Waiver:

- All storage requirements waived.  
 Post-development peak discharge rates do not exceed pre-development conditions.  
 Other:

Explain: \_\_\_\_\_  
\_\_\_\_\_

- Waiver approved per above conditions.**

---

Floodplain Administrator or Designee

---

Date

## **Stormwater Management Department**

7447 E Indian School Road, Suite 125, Scottsdale, AZ 85251 • Phone: 480-312-2500

# Request for Stormwater Storage Waiver



10-ZN-2020

**City of Scottsdale Plan/Case Numbers:**

- DR - \_\_\_\_\_

- PP - \_\_\_\_\_

PC# \_\_\_\_\_

## In-Lieu Fee and In-Kind Contributions

In-lieu fees are only applicable to projects where post-development peak discharge rates exceed pre-development levels, based on the 10- and 100-year storm events. If the city grants a waiver, the developer is required to calculate and contribute an in-lieu fee based on what it would cost the city to provide a storage basin, sized as described below, including costs such as land acquisition, construction, landscaping, design, construction management, and maintenance over a 75-year design life. The fee for this cost is \$3.00 per cubic foot of stormwater storage for a virtual storage basin designed to mitigate the increase in runoff associated with the 100-year/2-hour storm event. The applicant may submit site-specific in-lieu fee calculations subject to the Floodplain Administrator's approval.

The Floodplain Administrator considers in-kind contributions on a case-by-case basis. An in-kind contribution can serve as part of or instead of the calculated in-lieu fee. In-kind contributions must be stormwater-related and must constitute a public benefit. In-lieu fees and in-kind contributions are subject to the approval of the Floodplain Administrator or designee.

Project Name \_\_\_\_\_

The waived stormwater storage volume is calculated using a simplified approach as follows:

**V =  $\Delta CRA$ ; where**

V = stormwater storage volume required, in cubic feet,

$\Delta C$  = increase in weighted average runoff coefficient over disturbed area ( $C_{post} - C_{pre}$ ),

R = 100-year/2-hour precipitation depth, in feet (DSPM, Appendix 4-1D, page 11), and

A = area of disturbed ground, in square feet

Furthermore,

R = \_\_\_\_\_

$\Delta C$  = \_\_\_\_\_

A = \_\_\_\_\_

V = \_\_\_\_\_

$V_p$  = \_\_\_\_\_

$V_w$  = \_\_\_\_\_

An in-lieu fee will be paid, based on the following calculations and supporting documentation:

In-lieu fee (\$) =  $V_w$  (cu. ft.) x \$3.00 per cubic foot = \_\_\_\_\_

An in-kind contribution will be made, as follows:

\_\_\_\_\_

No in-lieu fee is required. Reason:

\_\_\_\_\_

**Approved by:**

Floodplain Administrator or Designee

Date

## Stormwater Management Department

7447 E Indian School Road, Suite 125, Scottsdale, AZ 85251 • Phone: 480-312-2500